

85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

August 16, 2017

Town of Stratham Planning Board Attn. Robert Baskerville, PE, Chairman 10 Bunker Hill Avenue Stratham, NH 03885

RE: Response Letter
Sullivan Subdivision Application
112 High Street
Tax Map 19, Lot 68
JBE Project No. 13070.1

Dear Chairman Baskerville and Members of the Board,

Jones & Beach Engineers, Inc. respectfully submits revisions to the Subdivision for the above-referenced parcel on behalf of property owner Robin Sullivan. The intent of this project is to construct a 5-lot residential subdivision, with 1,134 L.F. of roadway and cul-de-sac from High Street. This project will be serviced with on-site wells and septic systems. We have sent plans and calculations to Civil Works for engineering review. We ask to postpone the next Public Hearing from September 6 to September 20.

The following changes have been made to the plans:

- 1. The road hammerhead layout has been revised to a 16' wide cul-de-sac, with new driveway locations. The Waiver Request is revised.
- 2. The detention pond and grading have been revised. The cul-de-sac is sloped to the center.
- 3. The Brockelbank shed is shown.
- 4. Note 22 was added to Sheet C2 indicating that the proposed Rain Gardens are to be constructed on each house lot (not for the road). Sample language to be placed in the deed for each lot is attached:

The Town of Stratham Planning Board approval requires an individual rain garden as shown on the herein referenced plan be constructed, owned, and maintained on each lot in accordance with best management practices as set forth by NH DES, which shall be constructed in accordance with Detail Sheet D2. Said individual rain garden shall be a minimum of 1,000 square feet with a 6" deep ponding area.

- 5. Soil Based Lot Size calculations are provided, therefore that Waiver Request is withdrawn.
- 6. Our wetland scientist has reevaluated the site, due to concern raised from the abutter in a thickly wooded area.

7. The required sight distance is shown on Sheet C2.

The following items are as revised:

- 1. Postponement Letter.
- 2. One (1) revised Waiver Request Form.
- 3. Soil Based Lot Sizing Calculations.
- 4. Three (3) bound copies of the revised drainage analysis.
- 5. Nine (9) complete reduced-size (11"x17") plan sets.
- 6. Six (6) complete full-size plan sets.

If you have any questions or need any additional information, please feel free to contact our office. Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Jonathan S. Ring, P.E. Son

President

cc: Robin Sullivan (via email)

Paul Connolly, Civil Works (via email, including application)



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

August 16, 2017

Town of Stratham Planning Board Attn: Robert Baskerville, Chairman 10 Bunker Hill Avenue Stratham, NH 03885

RE: Planning Board Postponement Letter

112 High Street, Stratham, NH

Tax Map 19, Lot 68 JBE Project No. 13070.1

Dear Board Members:

On behalf of our client, Robin Sullivan, Jones & Beach Engineers, Inc. respectfully requests a continuance of the pending application for the above-referenced parcel from the September 6th hearing to the September 20th meeting. We also grant a 30-day extension to the 65-day approval clock.

Please contact me if you have any questions. Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Jonathan S. Ring, PE Jonathan S. Ring, PE

President

ce: Robin Sullivan



TOWN OF STRATHAM

10 Bunker Hill Avenue · Stratham, NH 03885 Phone: 603-772-7391 Fax (All Offices) 603-775-0517

SITE PLAN REVIEW / SUBDIVISION WAIVER REQUEST FORM

Name of Subdivision/Site Plan: Proposed Sullivan Subdivison
Street Address: 112 High Street, Stratham, NH
I Robin Sullivan hereby request that the Planning Board waive the requirements of item(s) Addendum A, Table 1. Roadway Pavement Width of 24' of the Subdivision/Site Plan Checklist in reference to a plan presented by Jones & Beach Engineers, Inc., Attn. Jonathan S. Ring, P.E. (name of surveyor and engineer) dated rev. August 16, 2017 for the property tax map(s) 19 and lot(s) in the Town of Stratham, NH
As the aforementioned applicant, I, herein, acknowledge that this waiver is requested in accordance with the provisions set forth in RSA 674:36, II (n) (For Subdivisions) OR RSA 674:44, III (e) (For Site-Plans). Without the Planning Board granting said waiver, strict conformity would cause an unnecessary hardship to the applicant and waiver would not be contrary to the spirit and intent of the regulations, CR, the specific circumstances relative to the subdivision/site plan or conditions of the land in the subdivision/site plan indicate that the waiver will properly carry out the spirit and intent of the regulations.
Strict conformity would cause an <u>unnecessary hardship</u> to the applicant and waiver would not be contrary to the spirit and intent of the regulations:
OR:
Specific circumstances relative to the subdivision or conditions of the land in the subdivision indicate that the waiver will properly <u>carry out the spirit and intent of the regulations</u> : We respectfully request a waiver from the 24' roadway width. In lieu of a 24' wide roadway, we propose a 22' wide
roadway with 16' wide cul-de-sac due to only five (5) lots that will access through the proposed roadway. Limited traffic will utilize the proposed roadway.
Signed: Applicant or Authorized Agent Planning Board Action:
Waiver Granted
Waiver Not Granted

J/B

LOT SIZE BY SOIL CLASSIFICATION

J/B

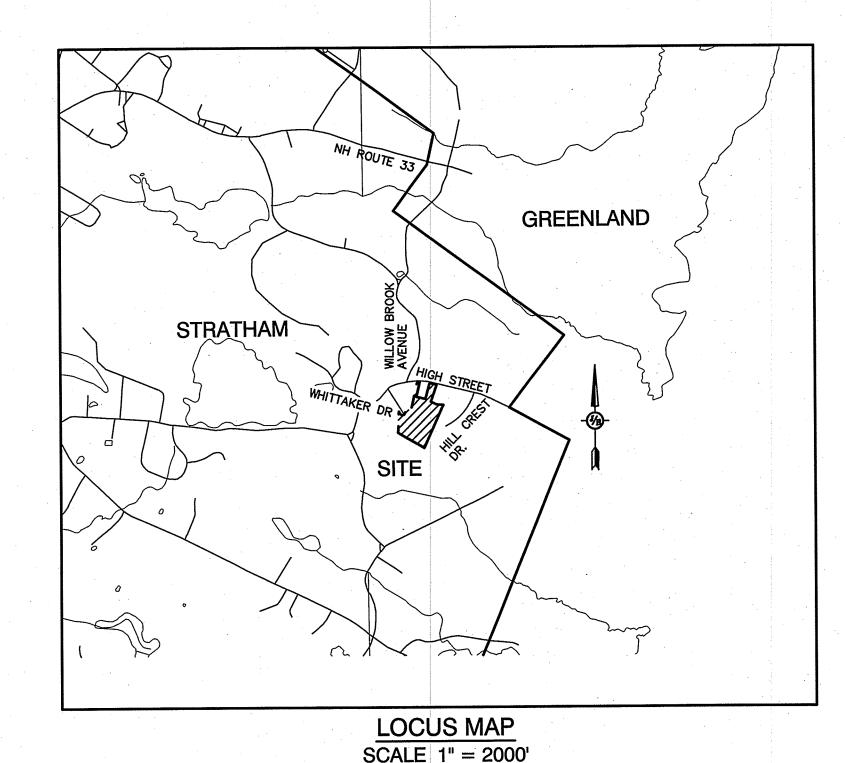
Sullivan Subdivision Robin Sullivan 112 High Street Stratham, NH 03885 JBE PROJECT NO. 13070 JONES & BEACH ENGINEERS INC. 85 PORTSMOUTH AVENUE P.O. BOX 219 STRATHAM, NH 03885 August 16, 2017

SOIL TYPE	HISS SOIL GROUP	SLOPE CATEGORY	TOWN REGULATION	SOIL AREA	WEIGHTED LOADING FACTOR
LOT 1 311CH 343BH TOTAL	3 3	C B	60,500 54,500	2,018 85,246 87,264	0.03 1.56 1.60
SOIL TYPE	HISS SOIL GROUP	SLOPE CATEGORY	TOWN REGULATION	SOIL AREA	WEIGHTED LOADING FACTOR
LOT 2 311BH 311CH 343BH 411BH 443BH 543BH TOTAL	3 3 4 4 5	B C B B B	54,500 60,500 54,500 77,000 77,000 106,000	47,432 15,959 5,434 1,697 14,514 9,061 94,097	0.87 0.26 0.10 0.02 0.19 0.09 1.53
SOIL TYPE	HISS SOIL GROUP	SLOPE CATEGORY	TOWN REGULATION	SOIL AREA	WEIGHTED LOADING FACTOR
LOT 3 311BH 311CH 343BH 411BH 443BH 543BH TOTAL	3 3 3 4 4 5	В С В В В В	54,500 60,500 54,500 77,000 77,000 106,000	6,466 9,601 37,345 12,575 11,111 21,417 98,515	0.12 0.16 0.69 0.16 0.14 0.20 1.47

SOIL TYPE	HISS SOIL GROUP	SLOPE CATEGORY	TOWN REGULATION	SOIL AREA	WEIGHTED LOADING FACTOR
LOT 4 311CH 343BH 411BH 511BH 543BH	3 3 4 5 5	С В В В	60,500 54,500 77,000 106,000 106,000	6,405 50,679 19,246 495 18,067 94,892	0.11 0.93 0.25 0.00 0.17 1.46
SOIL TYPE	HISS SOIL GROUP	SLOPE CATEGORY	TOWN REGULATION	SOIL AREA	WEIGHTED LOADING FACTOR
LOT 5 311BH 311CH 343BH 411BH 511BH 543BH TOTAL	3 3 4 5 5	B C B B B B	54,500 60,500 54,500 77,000 106,000 106,000	18,264 26,117 26,440 14,003 3,443 325 88,592	0.34 0.43 0.49 0.18 0.03 0.00 1.47

GENERAL LEGEND FRESHWATER WETLANDS LINE MAJOR CONTOUR MINOR CONTOUR EDGE OF PAVEMENT SILT FENCE DRAINAGE LINE OVERHEAD ELECTRIC JNDERGROUND ELECTRIC GUARDRAIL IRON PIPE/IRON ROD DRILL HOLE IRON ROD/DRILL HOLE STONE/GRANITE BOUND 100x0 SPOT GRADE x 100.00 PAVEMENT SPOT GRADE CURB SPOT GRADE BENCHMARK (TBM) DOUBLE POST SIGN SINGLE POST SIGN TEST PIT FAILED TEST PIT MONITORING WELL PERC TEST PHOTO LOCATION TREES AND BUSHES UTILITY POLE LIGHT POLES DRAIN MANHOLE SINGLE GRATE CATCH BASIN DOUBLE GRATE CATCH BASIN TRANSFORMER CULVERT W/WINGWALLS CULVERT W/FLARED END SECTION CULVERT W/STRAIGHT HEADWALL STONE CHECK DAM DRAINAGE FLOW DIRECTION 4K SEPTIC AREA VEGETATED FILTER STRIP D&D&D&Q **RIPRAP** जींक जींक जींक FRESHWATER WETLANDS STABILIZED CONSTRUCTION ENTRANCE CONCRETE GRAVEL SNOW STORAGE

SULLIVAN SUBDIVISION PLAN TAX MAP 19 AND LOT 68 112 HIGH STREET, STRATHAM, NH 03885



SHEET INDEX

COVER SHEET

A1 SUBDIVISION PLAN

EXISTING CONDITIONS PLAN

C2 GRADING AND DRAINAGE PLAN

P1 PLAN AND PROFILE

D1-D2 DETAIL SHEETS

1 EROSION AND SEDIMENT CONTROL DETAILS

CIVIL ENGINEER/WETLANDS

JONES & BEACH ENGINEERS, INC. 85 PORTSMOUTH AVENUE PO BOX 219 STRATHAM, NH 03885 (603) 772-4746 CONTACT: JONATHAN RING, PE. EMAIL: JRING@JONESANDBEACH.COM

OWNER OF RECORD

ROBIN SULLIVAN 8 WHITTAKER DRIVE STRATHAM, NH 03885

SOIL CONSULTANT

GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTIAL DRIVE, UNIT H EXETER, NH 03833-7507 (603) 778-0644 CONTACT: JIM GOVE **SURVEYOR**

JAMES VERRA AND ASSOCIATES, INC.
101 SHATTUCK WAY, SUITE 8
NEWINGTON, NH 03801
(603) 436-3557
CONTACT: JAMES VERRA
EMAIL: JAMESV@JVASURVEYORS.COM

Stratham, NH 03885

ELECTRIC

UNITIL 6 LIBERTY LANE WEST HAMPTON, NH 03842 (800) 852-7276 **TELEPHONE**

FAIRPOINT COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (603) 427-5525 CONTACT: JOE CONSIDINE

CABLE TV
COMCAST COMMUNICATION CORPORATION
334-B CALEF HIGHWAY
EPPING, NH 03042-2325
(603) 679-5695

E-MAIL: JBE@JONESANDBEACH.COM

PROJECT PARCEL
TOWN OF STRATHAM, NH
MAP 19, LOT 68

APPLICANT/OWNER

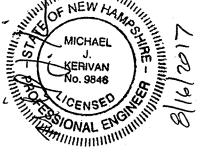
ROBIN SULLIVAN 8 WHITTAKER DRIVE STRATHAM, NH 03885 BK 4199 PG 2969

TOTAL LOT AREA 14.99 ACRES

APPROVED - STRATHAM, NH PLANNING BOARD

DATE:

Design: JSR Draft: PLB Date: 6/26/13
Checked: JSR Scale: AS NOTED Project No.: 13070.1
Drawing Name: 13070-PLAN.dwg
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



	·			
	2	8/16/17	REVISED PER PLANNING BOARD	LAZ
	1	7/5/17	REVISED PER TOWN PLANNER	RMN
-	0	6/29/17	REVISED FOR PLANNING BOARD	PLB
	REV.	DATE	REVISION	BY

Bones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services

603-772-4746
FAX: 603-772-0227

Plan Name:

COVER SHEET

SULLIVAN SUBDIVISION
112 HIGH STREET,STRATHAM, NH 03885

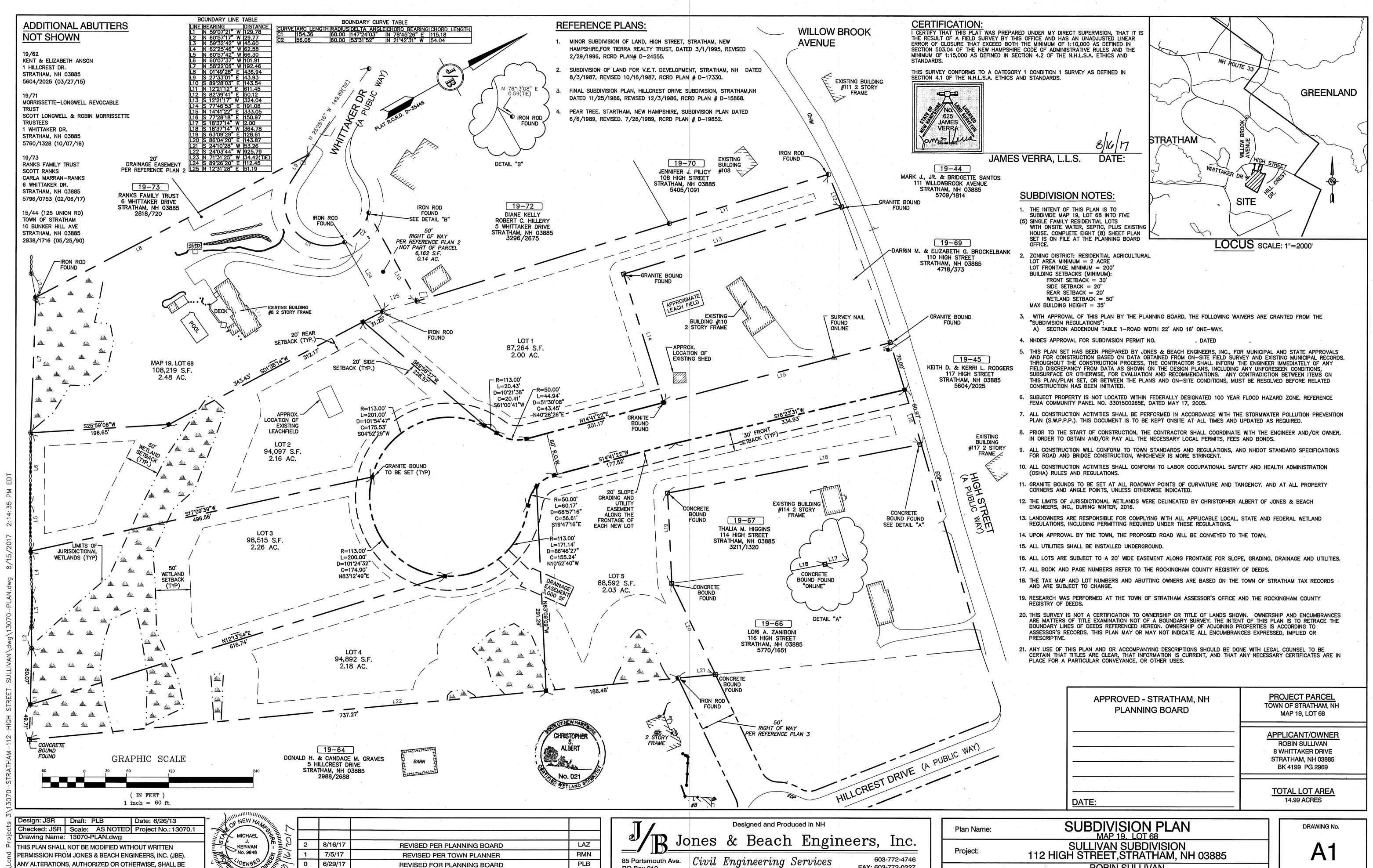
ROBIN SULLIVAN
8 WHITTAKER DRIVE, STRATHAM, NH 03885

DRAWING No.

CS

SHEET 1 OF 8

JBE PROJECT NO. 13070.1



ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

(CENSE)

6/29/17

DATE

REVISED FOR PLANNING BOARD

REVISION

PLB

BY

PO Box 219

Stratham, NH 03885

A SHEET 2 OF 8 JBE PROJECT NO. 13070.1

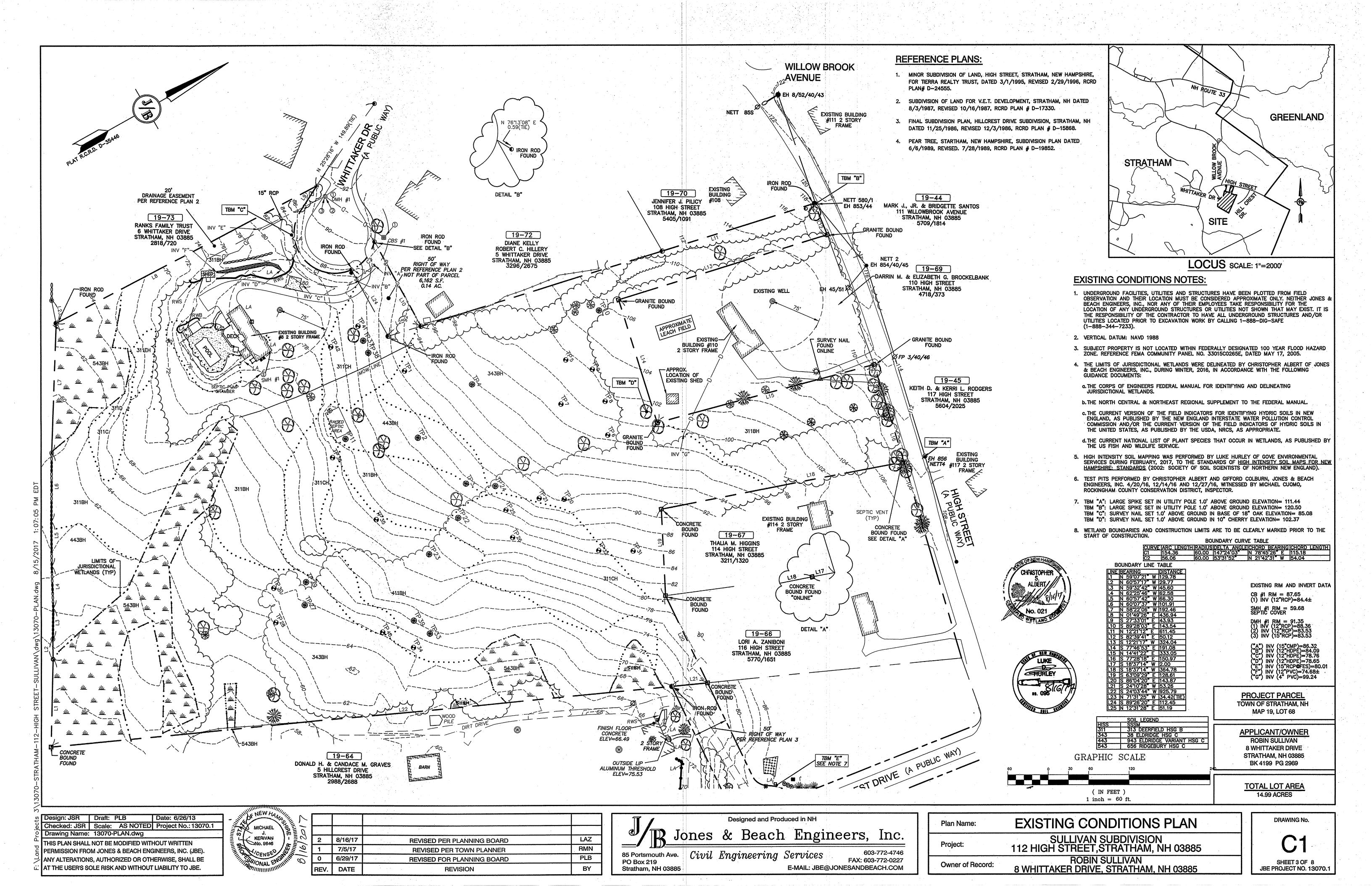
ROBIN SULLIVAN

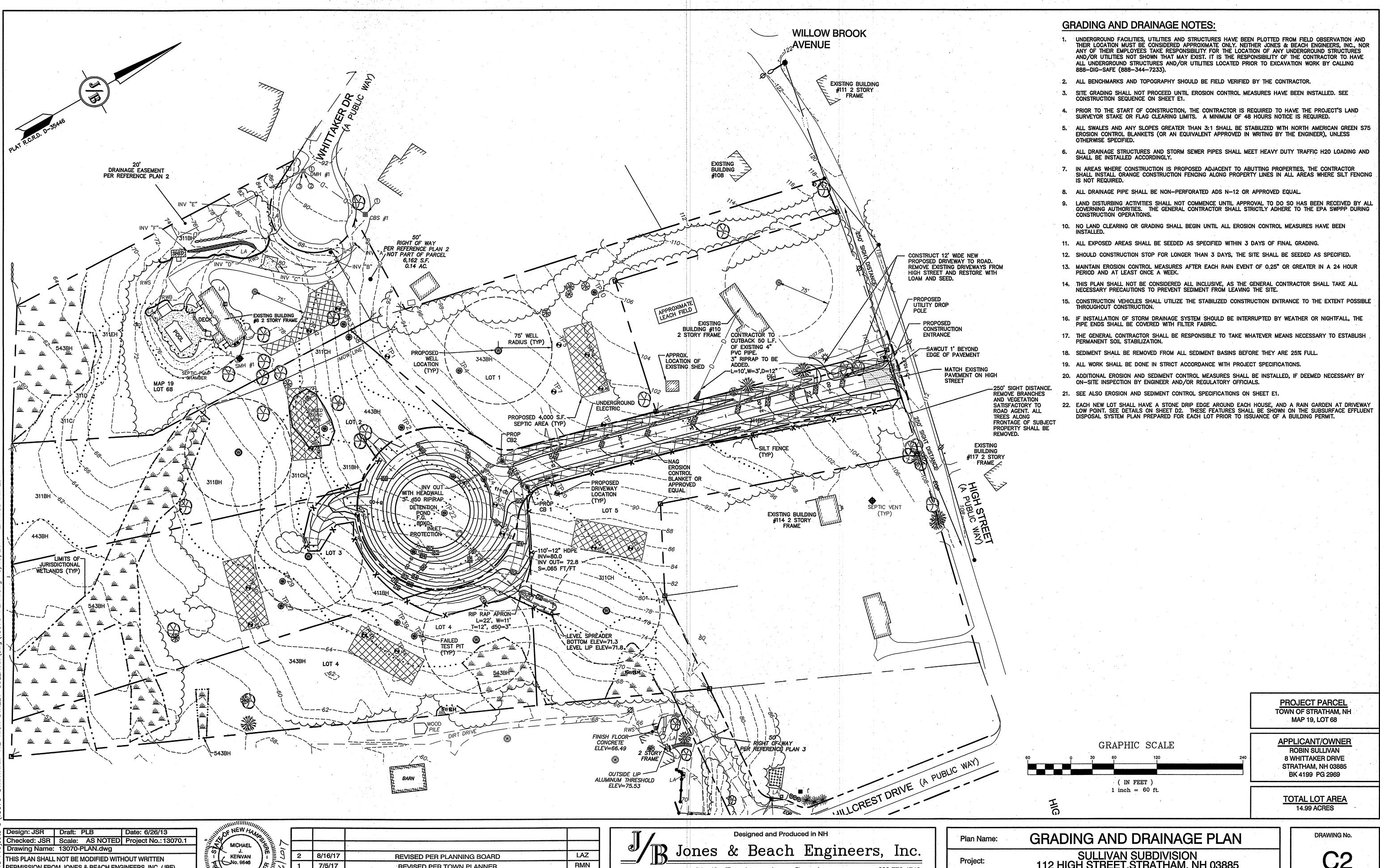
8 WHITTAKER DRIVE, STRATHAM, NH 03885

FAX: 603-772-0227

E-MAIL: JBE@JONESANDBEACH.COM

Owner of Record:





ERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE) ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

No. 9848 7/5/17 **REVISED PER TOWN PLANNER** 0 6/29/17 REVISED FOR PLANNING BOARD DATE REVISION

PLB

BY

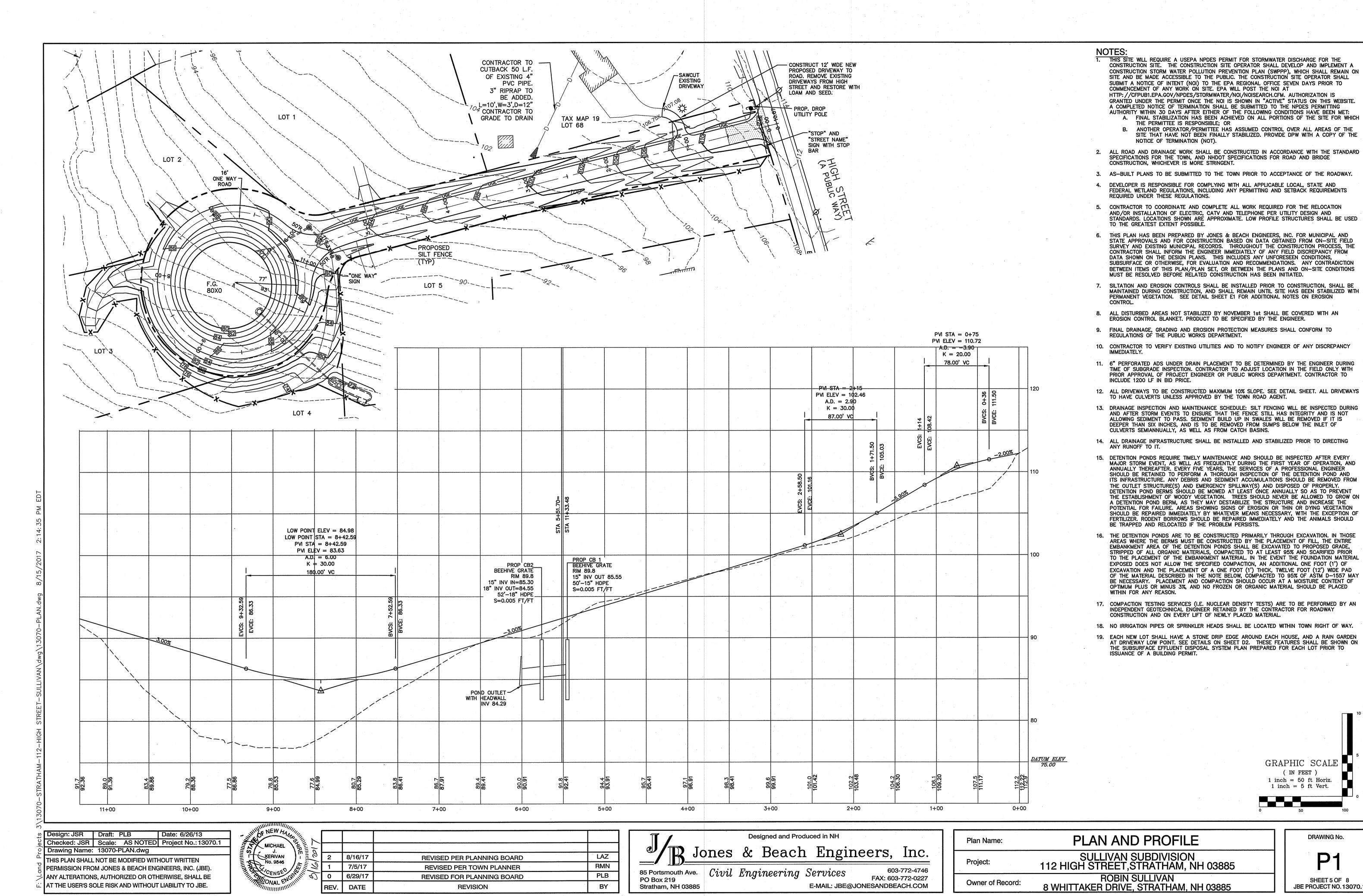
Stratham, NH 03885

Civil Engineering Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

SULLIVAN SUBDIVISION 112 HIGH STREET,STRATHAM, NH 03885 ROBIN SULLIVAN 8 WHITTAKER DRIVE, STRATHAM, NH 03885

Owner of Record:

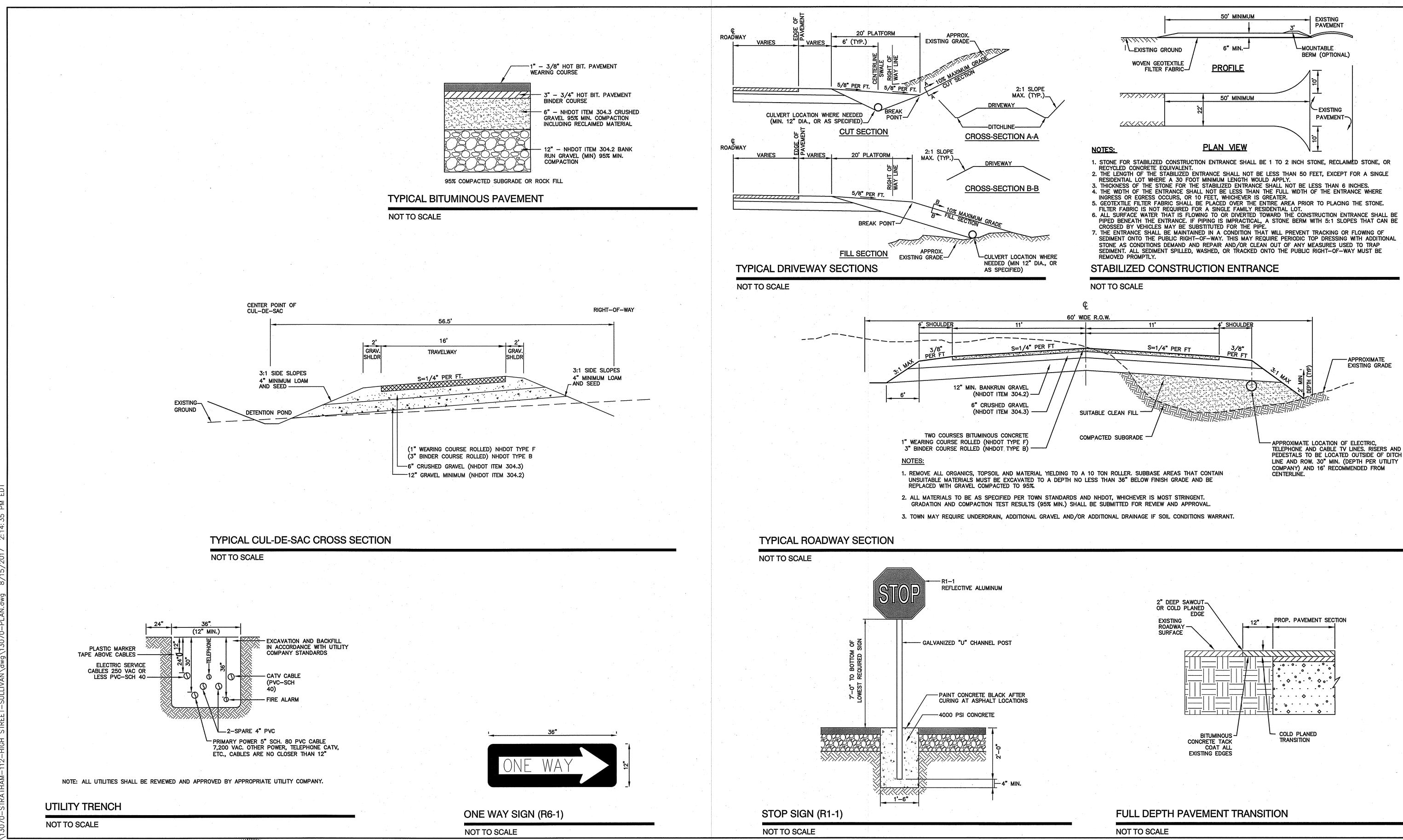
SHEET 4 OF 8 **JBE PROJECT NO. 13070.1**



P SHEET 5 OF 8 **JBE PROJECT NO. 13070.1**

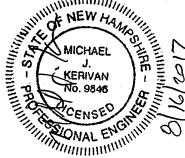
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GRAPHIC SCAL (IN FEET) 1 inch = 50 ft Horiz. 1 inch = 5 ft Vert.



3				
ţ	Design: JSR	Draft: PLB	Date: 6/26/13]
ojec	Checked: JSR		Project No.: 13070.1] 3
<u> </u>		13070-PLAN.dwg] 🖹
- σ	THIS PLAN SHALL	NOT BE MODIFIED WITH DM JONES & BEACH ENG	HOUT WRITTEN	
and	PERMISSION FRO	OM JONES & BEACH ENG	SINEERS, INC. (JBE).	
Ĭ	ANY ALTERATION	S, AUTHORIZED OR OTH	HERWISE, SHALL BE	1
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AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



2	8/16/17	REVISED PER PLANNING BOARD	LAZ
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0	6/29/17	REVISED FOR PLANNING BOARD	PLB
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	2 1 0 REV.	1 7/5/17 0 6/29/17	1 7/5/17 REVISED PER TOWN PLANNER 0 6/29/17 REVISED FOR PLANNING BOARD

Designed and Produced in NH

Jones & Beach Engineers, Inc.

85 Portsmouth Ave.
PO Box 219
Stratham, NH 03885

Designed and Produced in NH

Engineering Services

603-772-4746
FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:

DETAIL SHEET

SULLIVAN SUBDIVISION
112 HIGH STREET,STRATHAM, NH 03885

ROBIN SULLIVAN
8 WHITTAKER DRIVE, STRATHAM, NH 03885

D1

SHEET 6 OF 8

JBE PROJECT NO. 13070.1

DRAWING No.

TYPICAL RAIN GARDEN PLANTINGS

BOTANICAL NAME	COMMON NAME	SIZE
PERENNIALS		
"ANNABELLE" HYDRANGEA HEMEROCALLIS 'STELLA D'ORO' VIBURNUM TRILOBUM	HYDRANGEA DAYLILY AMERICAN CRANBERRY	1 GAL. 1 GAL. 1 GAL.
AUREA BOWLES' GOLDEN SEDGE SPIREA	SEDGE GRASS BRIDLE VEIL	1 GAL. 1 GAL.

DECIDUOUS SHRUBS:

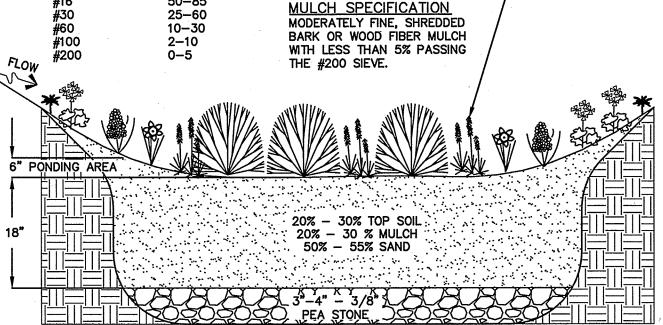
VIBURNUM DENTATUM ALNUS INCANA CORNUS STOLONIFERA VACCINIUM CORYMBOSUM LLEX VERTICILLATA

ARROWOOD VIBURNUM SPECKLED ALDER REDOSIER DOGWOOD HIGHBUSH BLUEBERRY **WINTERBERRY**

SAND SPECIFICATION SIEVE SIZE % BY W

TOPSOIL SPECIFICATION LOAMY SAND TOPSOIL WITH MINIMAL CLAY CONTENT AND BETWEEN 15 TO 25% FINES PASSING THE #200 SIEVE.

-NATIVE SHRUB AND PERENNIAL PLANTINGS



DESIGN CONSIDERATIONS

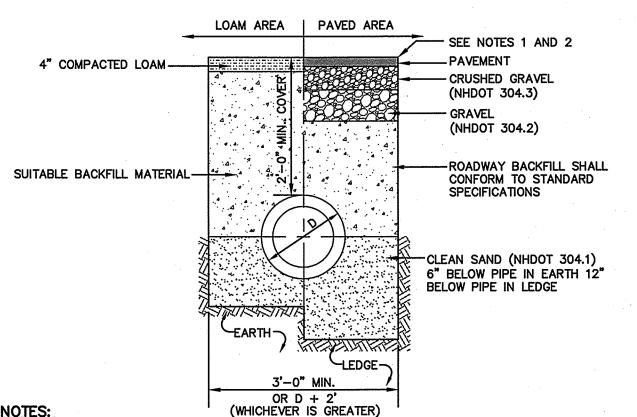
- DO NOT DIRECT RUNOFF TO THE BIORETENTION SYSTEMS UNTIL IT HAS BEEN PLANTED AND ITS CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED.
- 2. DO NOT DISCHARGE SEDIMENT-LADEN WATERS FROM CONSTRUCTION ACTIVITIES (RUN-OFF, WATER FROM EXCAVATIONS) TO THE BIORETENTION AREA DURING ANY STAGE OF CONSTRUCTION.
- DO NOT TRAFFIC EXPOSED SOIL SURFACE WITH CONSTRUCTION EQUIPMENT. IF FEASIBLE, PERFORM EXCAVATIONS WITH EQUIPMENT OUTSIDE THE LIMITS OF THE INFILTRATION COMPONENTS OF THE
- 4. PLANT LAYOUT WITHIN INDIVIDUAL RAIN GARDENS MAY VARY BETWEEN HOMES HOWEVER ALL RAIN GARDENS ARE TO BE PLANTED FROM EDGE TO EDGE WITH A 1' MAXIMUM SPACING BETWEEN PERENNIALS. LEAVE ENOUGH ROOM BETWEEN SHRUBS FOR FULL GROW-OUT OF EACH SPECIES USED.

MAINTENANCE REQUIREMENTS:

VEGETATION SHOULD BE INSPECTED AT LEAST ANNUALLY, AND MAINTAINED IN HEALTHY CONDITION, OF INVASIVE SPECIES.

RAIN GARDEN (with open side and bottom) - HOUSE LOTS

NOT TO SCALE

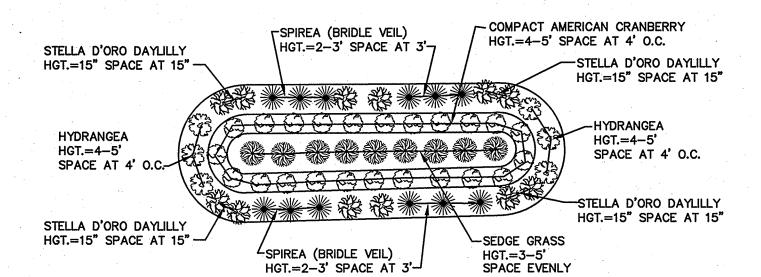


NOTES:

- 1. PAVEMENT REPAIR IN EXISTING ROADWAYS SHALL CONFORM TO STREET OPENING REGULATIONS.
- 2. NEW ROADWAY CONSTRUCTION SHALL CONFORM WITH PROJECT AND TOWN SPECIFICATIONS.
- 3. ALL MATERIALS ARE TO BE COMPACTED TO 95% OF ASTM D-1557.

DRAINAGE TRENCH

NOT TO SCALE

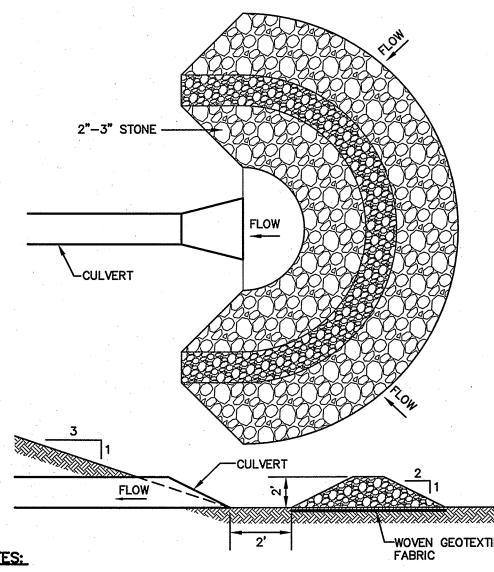


ELEVATIONS VARY BY LOT. CONTRACTOR TO PLACE RAIN GARDENS ON EACH RESIDENTIAL LOT AND PLANT AS SHOWN ABOVE. SHAPE AND DIMENSIONS MAY VARY DEPENDING ON SITE CONDITIONS.

- 2. RAIN GARDENS TO BE 75' MINIMUM FROM SEPTIC SYSTEMS.
- 3. DRIVEWAY RUNOFF MUST BE DIRECTED INTO PROPOSED RAIN GARDENS.
- 4. BOTTOM OF RAIN GARDEN TO BE A MINIMUM 1,000 S.F. SHAPE AND DIMENSIONS MAY VARY DUE TO SITE CONDITIONS.
- 5. VEGETATION WITHIN EACH RAIN GARDEN MUST BE STABILIZED WITH GROWTH PRIOR TO DIRECTING RUNOFF INTO THE RAIN GARDEN.

TYPICAL RAIN GARDEN PLANTINGS - HOUSE LOTS

NOT TO SCALE

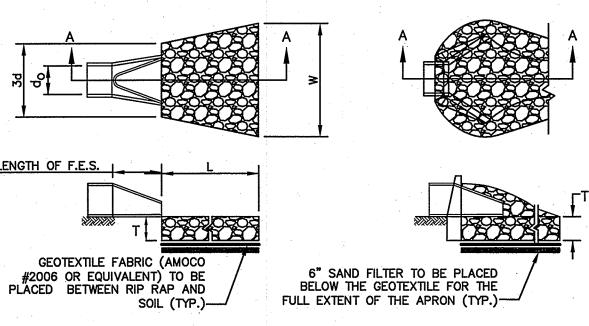


NOTES:

- 1. TEMPORARY CULVERT INLET PROTECTION CHECK DAMS SHALL BE CONSTRUCTED OF 2-3"
- 2. INLET PROTECTION MEASURES SHALL BE INSTALLED AT THE OPENINGS OF ALL EXISTING AND PROPOSED CULVERTS LOCATED BELOW (DOWNSTREAM) FROM AND WITHIN 100' OF THE
- 3. SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURE WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.
- 4. STRUCTURES SHALL BE REMOVED WHEN THE SITE IS STABILIZED WITH VEGETATION AND THE CHANNEL SHALL BE SMOOTHED AND REVEGETATED.

TEMPORARY CULVERT INLET PROTECTION CHECK DAM

NOT TO SCALE



SECTION A-A PIPE OUTLET TO FLAT AREA WITH NO DEFINED CHANNEL

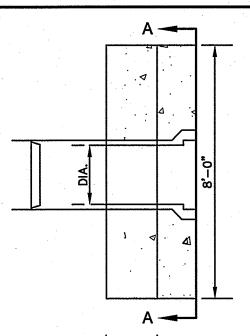
PIPE OUTLET TO WELL-DEFINED CHANNEL

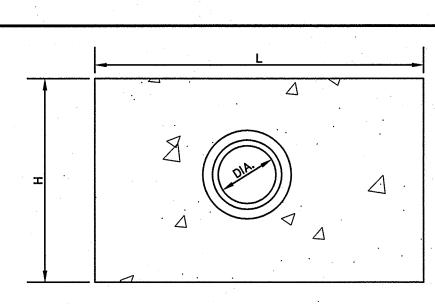
				* The second of			
ABLE 7-24-	-RECOMME	NDED R	IP RAP	GRADAT	ION RANG	ES	
HICKNESS OF RI	P RAP = 1.	O FEET		, -			
50 SIZE=	0.25	FEET	. 3	INCHES			
OF WEIGHT SMA			SIZE (OF STONE (INCHES) TO		
100%			5		6		
85%			4	* .	5	6	
50%		1	3		5	5	
15%	*		1		2	2	

- 1. THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIP RAP SHALL BE PREPARED TO THE LINES AND GRADES SHOWN ON THE PLANS.
- 2. THE RIP RAP SHALL CONFORM TO THE SPECIFIED GRADATION.
- 3. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE ROCK RIP. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC, ALL OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 12 INCHES.
- 4. STONE FOR THE RIP RAP MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE
- 5. OUTLETS TO A DEFINED CHANNEL SHALL HAVE 2:1 OR FLATTER SIDE SLOPES AND SHOULD BEGIN AT THE TOP OF THE CULVERT AND TAPER DOWN TO THE CHANNEL BOTTOM THROUGH THE LENGTH OF THE
- 6. MAINTENANCE; THE OUTLET PROTECTION SHOULD BE CHECKED AT LEAST ANNUALLY AND AFTER EVERY MAJOR STORM. IF THE RIP RAP HAS BEEN DISPLACED, UNDERMINED OR DAMAGED, IT SHOULD BE REPAIRED IMMEDIATELY. THE CHANNEL IMMEDIATELY BELOW THE OUTLET SHOULD BE CHECKED TO SEE THAT ROOM IS NOT OCCUPRING. THE DEPOSIT AND SEPREFALL THAT COME BY DATE THAT OBSTRUCTIONS SUCH AS FALLEN TREES, DEBRIS, AND SEDIMENT THAT COULD CHANGE FLOW PATTERNS AND/OR TAILWATER DEPTHS ON THE PIPES. REPAIRS MUST BE CARRIED OUT IMMEDIATELY TO AVOID ADDITIONAL DAMAGE TO OUTLET PROTECTION.

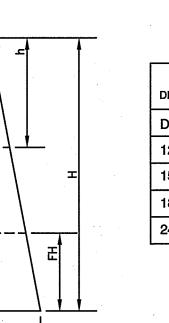
RIP RAP OUTLET PROTECTION APRON

NOT TO SCALE





SECTION A-A



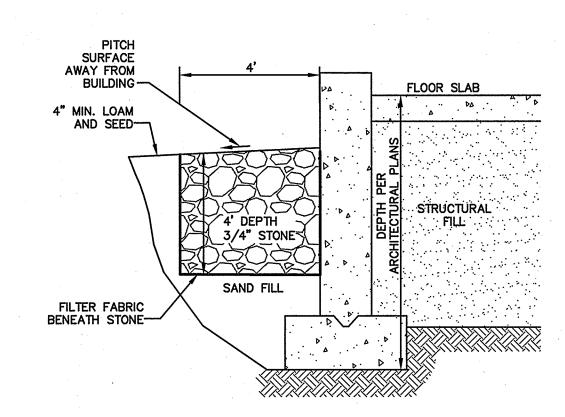
DIA.	HEADWALL LENGTH	HEADWALL HEIGHT	FILL HEIGHT	PIPE COVER	HEADWALL BOTTOM WIDTH
D	L	Н	FH	h	w
12"	4'-2"	3'-9"	1'-6"	1'-3"	1'-11"
15"	5'-11"	4'-2"	1'-6"	1'-5"	2'-0"
18"	6'-11"	4'-5"	1'-6"	1'-5"	2'-1"
24"	8'-10"	4'-11"	1'6"	1'-5"	2'-3"

LONGITUDINAL SECTION

- ALL DIMENSIONS GIVEN IN FEET & INCHES.
- 2. PROVIDE BELL END AT INLET HEADWALL, AND SPIGOT END AT OUTLET END HEADWALL.
 3. CONCRETE: 5,000 PSI MINIMUM AFTER 28 DAYS. CEMENT TO BE TYPE III PER ASTM C-150. REINFORCING TO MEET OR EXCEED ASTM A-615 GRADE 60 DEFORMED BARS.
- 4. 1" THREADED INSERTS PROVED FOR FINAL ATTACHMENT IN FIELD BY OTHERS.

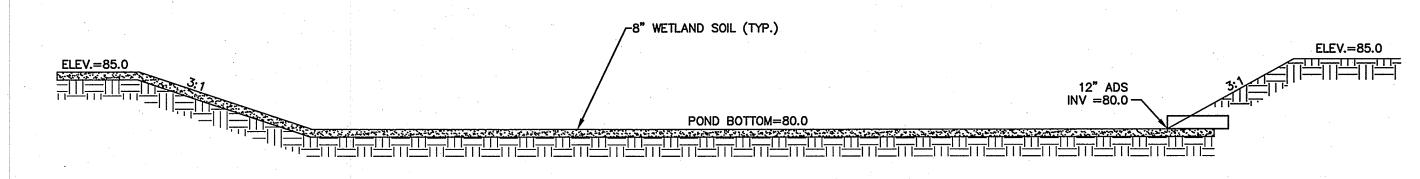
PRECAST CONCRETE HEADWALL

NOT TO SCALE



STONE DRIP EDGE DETAIL

NOT TO SCALE



CUL-DE-SAC DETENTION POND SYSTEM SECTION

NOT TO SCALE

Design: JSR Draft: PLB Date: 6/26/13 Checked: JSR | Scale: AS NOTED | Project No.: 13070.1 Drawing Name: 13070-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



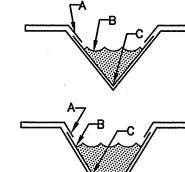
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2	8/16/17	REVISED PER PLANNING BOARD	LAZ
1	7/5/17	REVISED PER TOWN PLANNER	RMN
0	6/29/17	REVISED FOR PLANNING BOARD	PLB
REV.	DATE	REVISION	BY

Designed and Produced in NH Jones & Beach Engineers, Inc. 85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-0227 PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

Plan Name:	DETAIL SHEET
Project:	SULLIVAN SUBDIVISION 112 HIGH STREET,STRATHAM, NH 03885
Owner of Record:	ROBIN SULLIVAN 8 WHITTAKER DRIVE, STRATHAM, NH 03885

DRAWING No. SHEET 7 OF 8 JBE PROJECT NO. 13070.1

- I. PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER, AND SEED. NOTE: WHEN USING CELL-O-SEED DO NOT SEED PREPARED AREA. CELL-O-SEED MUST BE INSTALLED WITH PAPER SIDE DOWN.
- 2. BEGIN AT THE TOP OF THE CHANNEL BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL CENTER BLANKET IN DIRECTION OF WATER FLOW IN BOTTOM OF CHANNEL. BLANKETS WILL UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE. WHEN USING OPTIONAL DOT SYSTEM, STAPLES/STAKES SHOULD BE PLACED THROUGH EACH OF THE COLORED DOTS CORRESPONDING TO THE APPROPRIATE STAPLE PATTERN. 4. PLACE CONSECUTIVE BLANKETS END OVER END (SHINGLE STYLE) WITH A 4"-6" OVERLAP. USE A DOUBLE
- ROW OF STAPLES STAGGERED 4" APART AND 4" ON CENTER TO SECURE BLANKETS. 5. FULL LENGTH EDGE OF BLANKETS AT TOP OF SIDE SLOPES MUST BE ANCHORED WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN A 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.
- 6. ADJACENT BLANKETS MUST BE OVERLAPPED APPROXIMATELY 2"-5" (DEPENDING ON BLANKET TYPE) AND STAPLED, TO INSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE BLANKET BEING OVERLAPPED. 7. IN HIGH FLOW CHANNEL APPLICATIONS, A STAPLE CHECK SLOT IS RECOMMENDED AT 30 TO 40 FOOT INTERVALS. USE A DOUBLE ROW OF STAPLES STAGGERED 4" APART AND 4" ON CENTER OVER ENTIRE WIDTH
- 8. THE TERMINAL END OF THE BLANKETS MUST BE ANCHORED WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN A 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.



OF THE CHANNEL.

<u>CRITICAL POINTS:</u>

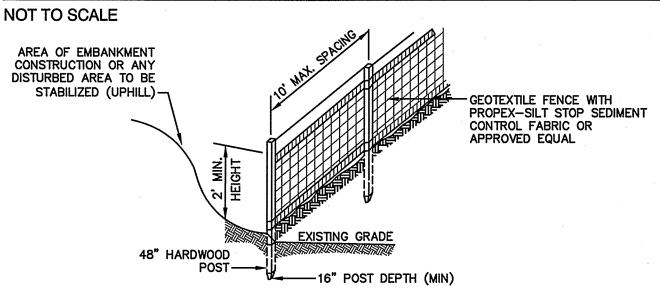
A. OVERLAPS AND SEAMS **B. PROJECTED WATER LINE**

C. CHANNEL BOTTOM/SIDE SLOPE VERTICES

* HORIZONTAL STAPLE SPACING SHOULD BE ALTERED IF NECESSARY TO ALLOW STAPLES TO SECURE THE CRITICAL POINTS ALONG THE CHANNEL

** IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY ANCHOR THE BLANKETS.

EROSION CONTROL BLANKET SWALE INSTALLATION NORTH AMERICAN GREEN (800) 772-2040



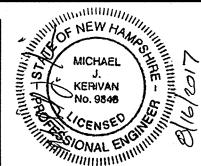
CONSTRUCTION SPECIFICATIONS:

- WOVEN FABRIC FENCE TO BE FASTENED SECURELY TO FENCE POSTS WITH WIRE TIES OR STAPLES. FILTER CLOTH SHALL BE FASTENED TO WOVEN WIRE EVERY 24" AT TOP, MID AND BOTTOM AND EMBEDDED IN THE GROUND A MINIMUM OF 8" AND THEN COVERED WITH SOIL.
- 2. THE FENCE POSTS SHALL BE A MINIMUM OF 48" LONG, SPACED A MAXIMUM 10' APART, AND DRIVEN A MINIMUM OF 16" INTO THE GROUND.
- 3. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER, THE ENDS OF THE FABRIC SHALL BE OVERLAPPED 6", FOLDED AND STAPLED TO PREVENT SEDIMENT FROM BY-PASSING.
- . MAINTENANCE SHALL BE PERFORMED AS NEEDED AND SEDIMENT REMOVED AND PROPERLY DISPOSED OF WHEN IT IS 6" DEEP OR VISIBLE 'BULGES' DEVELOP IN THE SILT FENCE.
- 5. PLACE THE ENDS OF THE SILT FENCE UP CONTOUR TO PROVIDE FOR SEDIMENT STORAGE.

SILT FENCE

NOT TO SCALE

Design: JSR | Draft: PLB Date: 6/26/13 Checked: JSR | Scale: AS NOTED | Project No.: 13070.1 Drawing Name: 13070-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



8/16/17 **REVISED PER PLANNING BOARD** 7/5/17 **REVISED PER TOWN PLANNER** 6/29/17 REVISED FOR PLANNING BOARD DATE REVISION BY

SEEDING SPECIFICATIONS

. GRADING AND SHAPING

A. SLOPES SHALL NOT BE STEEPER THAN 2:1 WITHOUT APPROPRIATE EROSION CONTROL MEASURES AS SPECIFIED ON THE PLANS (3:1 SLOPES OR FLATTER ARE PREFERRED)

2. SEEDBED PREPARATION

A. SURFACE AND SEEPAGE WATER SHOULD BE DRAINED OR DIVERTED FROM THE SITE TO PREVENT DROWNING OR WINTER KILLING OF THE PLANTS.

B. STONES LARGER THAN 4 INCHES AND TRASH SHOULD BE REMOVED BECAUSE THEY INTERFERE WITH SEEDING AND FUTURE MAINTENANCE OF THE AREA. WHERE FEASIBLE, THE SOIL SHOULD BE TILLED TO A 4. DEPTH OF ABOUT 4 INCHES TO PREPARE A SEEDBED AND FERTILIZER AND LIME MIXED INTO THE SOIL. THE SEEDBED SHOULD BE LEFT IN A REASONABLY FIRM AND SMOOTH CONDITION. THE LAST TILLAGE OPERATION, SHOULD BE PERFORMED ACROSS THE SLOPE WHEREVER PRACTICAL.

3. ESTABLISHING A STAND

A. LIME AND FERTILIZER SHOULD BE APPLIED PRIOR TO OR AT THE TIME OF SEEDING AND INCORPORATED INTO THE SOIL. TYPES AND AMOUNTS OF LIME AND FERTILIZER SHOULD BE BASED ON AN EVALUATION OF SOIL TESTS. WHEN A SOIL TEST IS NOT AVAILABLE, THE FOLLOWING MINIMUM AMOUNTS SHOULD BE

AGRICULTURAL LIMESTONE, 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT. NITROGEN(N), 50 LBS. PER ACRE OR 1.1 LBS. PER 1,000 SQ.FT.

PHOSPHATE(P205), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT. POTASH(K20), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.

B. WHERE MOWING WILL BE DONE, 3:1 SLOPES OR FLATTER ARE RECOMMENDED.

(NOTE: THIS IS THE EQUIVALENT OF 500 LBS. PER ACRE OF 10-20-20 FERTILIZER OR 1,000 LBS. PER ACRE OF 5-10-10.)

- B. SEED SHOULD BE SPREAD UNIFORMLY BY THE METHOD MOST APPROPRIATE FOR THE SITE. METHODS INCLUDE BROADCASTING, DRILLING AND HYDROSEEDING. WHERE BROADCASTING IS USED, COVER SEED WITH .25 INCH OF SOIL OR LESS, BY CULTIPACKING OR RAKING.
- C. REFER TO THE 'SEEDING GUIDE' AND 'SEEDING RATES' TABLES ON THIS SHEET FOR APPROPRIATE SEED MIXTURES AND RATES OF SEEDING. ALL LEGUMES (CROWNVETCH, BIRDSFOOT, TREFOIL AND FLATPEA) MUST BE INOCULATED WITH THEIR SPECIFIC INOCULANT PRIOR TO THEIR INTRODUCTION TO THE SITE. WHEN SEEDED AREAS ARE MULCHED, PLANTINGS MAY BE MADE FROM EARLY SPRING TO EARLY OCTOBER.
- WHEN SEEDED AREAS ARE NOT MULCHED, PLANTINGS SHOULD BE MADE FROM EARLY SPRING TO MAY 20th OR FROM AUGUST 10th TO SEPTEMBER 1st.

- A. HAY, STRAW, OR OTHER MULCH, WHEN NEEDED, SHOULD BE APPLIED IMMEDIATELY AFTER SEEDING. B. MULCH WILL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE BEST MANAGEMENT PRACTICE
- FOR MULCHING. HAY OR STRAW MULCH SHALL BE PLACED AT A RATE OF 90 LBS PER 1000 S.F. 5. MAINTENANCE TO ESTABLISH A STAND
- A. PLANTED AREAS SHOULD BE PROTECTED FROM DAMAGE BY FIRE, GRAZING, TRAFFIC, AND DENSE WEED 12.
- B. FERTILIZATION NEEDS SHOULD BE DETERMINED BY ONSITE INSPECTIONS. SUPPLEMENTAL FERTILIZER IS USUALLY THE KEY TO FULLY COMPLETE THE ESTABLISHMENT OF THE STAND BECAUSE MOST PERENNIALS TAKE 2 TO 3 YEARS TO BECOME FULLY ESTABLISHED.
- C. IN WATERWAYS, CHANNELS, OR SWALES WHERE UNIFORM FLOW CONDITIONS ARE ANTICIPATED, ANNUAL MOWING MAY BE NECESSARY TO CONTROL GROWTH OF WOODY VEGETATION.

and the second s			1		
USE	SEEDING MIXTURE 1/	DROUGHTY	WELL DRAINED	MODERATELY WELL DRAINED	POORLY DRAINED
STEEP CUTS AND FILLS, BORROW AND DISPOSAL AREAS	A B C	FAIR POOR POOR	GOOD GOOD GOOD	GOOD FAIR EXCELLENT	FAIR FAIR GOOD
AREAS	D	FAIR	EXCELLENT	EXCELLENT	POOR
WATERWAYS, EMERGENG SPILLWAYS, AND OTHER CHANNELS WITH FLOWING WATER.		GOOD GOOD	GOOD EXCELLENT	GOOD EXCELLENT	FAIR FAIR
LIGHTLY USED PARKING LOTS, ODD AREAS, UNUSED LANDS, AND LOW INTENSITY USE RECREATION SITES.	A B C	GOOD GOOD GOOD	GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT	FAIR POOR FAIR
PLAY AREAS AND ATHLETIC FIELDS. (TOPSOIL IS ESSENTIAL FOR GOOD TURF.)	E F	FAIR FAIR	EXCELLENT EXCELLENT	EXCELLENT EXCELLENT	<u>2/</u> <u>2/</u>

GRAVEL PIT, SEE NH-PM-24 IN APPENDIX FOR RECOMMENDATION REGARDING RECLAMATION OF SAND AND GRAVEL PITS. / REFER TO SEEDING MIXTURES AND RATES IN TABLE BELOW.

NOTE: TEMPORARY SEED MIX FOR STABILIZATION OF TURF SHALL BE WINTER RYE OR OATS AT A RATE OF 2.5 LBS. PER 1000 S.F. AND SHALL BE PLACED PRIOR TO OCTOBER 15th, IF PERMANENT SEEDING NOT YET COMPLETE.

7 POORLY DRAINED SOILS ARE NOT DESIRABLE FOR USE AS PLAYING AREA AND ATHLETIC FIELDS.

SEEDING GUIDE

			•
	MIXTURE	POUNDS PER ACRE	POUNDS PER 1.000 Sq. Ft
	A. TALL FESCUE CREEPING RED FESCUE RED TOP TOTAL	20 20 2 42	0.45 0.45 <u>0.05</u> 0.95
	B. TALL FESCUE CREEPING RED FESCUE CROWN VETCH OR FLAT PEA TOTAL	15 10 15 30 40 OR 55	0.35 0.25 0.35 0.75 0.95 OR 1.35
*	C. TALL FESCUE CREEPING RED FESCUE BIRDS FOOT TREFOIL TOTAL	20 20 8 48	0.45 0.45 <u>0.20</u> 1.10
	D. TALL FESCUE FLAT PEA TOTAL	20 30 50	0.45 <u>0.75</u> 1.20
	E. CREEPING RED FESCUE 1/ KENTUCKY BLUEGRASS 1/ TOTAL	50 <u>50</u> 100	1.15 1.15 2.30
1.	F. TALL FESCUE 1	150	3.60
	1/ FOR HEAVY USE ATHLETIC FIELDS NEW HAMPSHIRE COOPERATIVE EXTEN CURRENT VARIETIES AND SEEDING RA	SION TURF SPE	
		4	

SEEDING RATES

TEMPORARY EROSION CONTROL NOTES

- 1. THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME. AT NO TIME SHALL AN AREA IN EXCESS OF 5 ACRES BE EXPOSED AT ANY ONE TIME BEFORE DISTURBED AREAS ARE STABILIZED.
- 2. EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS AND AT LOCATIONS AS REQUIRED, DIRECTED BY THE ENGINEER.
- 3. ALL DISTURBED AREAS (INCLUDING POND AREAS BELOW THE PROPOSED WATERLINE) SHALL BE RETURNED TO PROPOSED GRADES AND ELEVATIONS. DISTURBED AREAS SHALL BE LOAMED WITH A MINIMUM OF 6" OF SCREENED ORGANIC LOAM AND SEEDED WITH SEED MIXTURE 'C' AT A RATE NOT LESS THAN 1.10 POUNDS OF SEED PER 1,000 S.F. OF AREA (48 LBS. / ACRE).
- SILT FENCES AND OTHER BARRIERS SHALL BE INSPECTED EVERY SEVEN CALENDAR DAYS AND WITHIN 24 HOURS OF A RAINFALL OF 0.25" OR GREATER. ALL DAMAGED AREAS SHALL BE REPAIRED, AND SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED AND DISPOSED OF. AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSION CONTROL MEASURES SHALL BE REMOVED AND THE AREA DISTURBED BY THE REMOVAL SMOOTHED AND RE-VEGETATED.
- 6. AREAS MUST BE SEEDED AND MULCHED OR OTHERWISE PERMANENTLY STABILIZED WITHIN 3 DAYS OF FINAL GRADING, OR TEMPORARILY STABILIZED WITHIN 14 DAYS OF THE INITIAL DISTURBANCE OF SOIL. ALL AREAS SHALL BE STABILIZED WITHIN 45 DAYS OF INITIAL
- ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING NORTH AMERICAN GREEN S75 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER) ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE
- AFTER NOVEMBER 15th, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3" OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
- 10. AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:
 - a. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
 - b. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;
 - c. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH STONE OR RIPRAP HAS BEEN INSTALLED; OR

 - d. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
- REQUIREMENTS AND INTENT OF RSA 430:53 AND AGR 3800 RELATIVE TO INVASIVE SPECIES. PRIOR TO CONSTRUCTION, A PHASING PLAN THAT DELINEATES EACH PHASE OF THE PROJECT SHALL BE SUBMITTED. ALL TEMPORARY

SEDIMENT BASINS THAT WILL BE NEEDED FOR DEWATERING WORK AREAS SHALL BE LOCATED AND IDENTIFIED ON THIS PLAN.

FUGITIVE DUST CONTROL IS REQUIRED TO BE CONTROLLED IN ACCORDANCE WITH ENV-A 1000, AND THE PROJECT IS TO MEET THE

CONSTRUCTION SEQUENCE

- PRIOR TO THE START OF ANY ACTIVITY, IT IS THE RESPONSIBILITY OF THE SITE'S SITE DEVELOPER (OR OWNER) TO FILE A NOTICE OF INTENT (NOI) FORM WITH THE ENVIRONMENTAL PROTECTION AGENCY (EPA) IN ORDER TO GAIN COVERAGE UNDER THE NPDES GENERAL PERMIT FOR STORM WATER DISCHARGES FROM CONSTRUCTION ACTIVITIES. A PRE CONSTRUCTION MEETING IS TO BE HELD WITH ALL DEPARTMENT HEADS PRIOR TO THE START OF CONSTRUCTION.
- WETLAND BOUNDARIES ARE TO BE CLEARLY MARKED PRIOR TO THE START OF CONSTRUCTION. AT LEAST A TEMPORARY CULVERT OR ROADBED TO BE IN PLACE PRIOR TO THE START OF CONSTRUCTION.
- CUT AND REMOVE TREES IN CONSTRUCTION AREA AS REQUIRED OR DIRECTED.
- 4. INSTALL SILT FENCING, HAY BALES AND CONSTRUCTION ENTRANCES PRIOR TO THE START OF CONSTRUCTION. THESE ARE TO BE MAINTAINED UNTIL THE FINAL PAVEMENT SURFACING AND LANDSCAPING AREAS ARE ESTABLISHED
- CLEAR, CUT, GRUB AND DISPOSE OF DEBRIS IN APPROVED FACILITIES. THIS INCLUDES ANY REQUIRED DEMOLITION OF EXISTING STRUCTURES,
- CONSTRUCT AND/OR INSTALL TEMPORARY OR PERMANENT SEDIMENT AND/OR DETENTION BASIN(S) AS REQUIRED. THESE FACILITIES SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING RUN-OFF TO THEM.
- STRIP LOAM AND PAVEMENT, OR RECLAIM EXISTING PAVEMENT WITHIN LIMITS OF WORK PER THE RECOMMENDATIONS OF THE PROJECT ENGINEER AND STOCKPILE EXCESS MATERIAL. STABILIZE STOCKPILE AS NECESSARY.
- PERFORM PRELIMINARY SITE GRADING IN ACCORDANCE WITH THE PLANS.
- 9. PREPARE BUILDING PAD(S) TO ENABLE BUILDING CONSTRUCTION TO BEGIN.
- 10. INSTALL THE DRAINAGE SYSTEMS FIRST, THEN ANY OTHER UTILITIES IN ACCORDANCE WITH THE PLAN AND DETAILS. ANY CONFLICTS BETWEEN UTILITIES ARE TO BE RESOLVED WITH THE INVOLVEMENT AND APPROVAL OF THE ENGINEER.
- 11. ALL SWALES AND DRAINAGE STRUCTURES ARE TO BE CONSTRUCTED AND STABILIZED PRIOR TO HAVING RUN-OFF DIRECTED TO THEM.
- 12. STORMWATER FLOWS ARE NOT TO BE DIRECTED TO TREATMENT PRACTICES UNTIL ALL CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED.
- 13. DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINAGE DITCHES, CHECK DAMS, SEDIMENT TRAPS, ETC., TO PREVENT EROSION ON THE SITE AND PREVENT ANY SILTATION OF ABUTTING WATERS AND/OR PROPERTY.
- 14. PERFORM FINAL FINE GRADING, INCLUDING PLACEMENT OF 'SELECT' SUBGRADE MATERIALS.
- 15. PAVE ALL ROADWAYS WITH INITIAL 'BASE COURSE'.
- 16. PERFORM ALL REMAINING SITE CONSTRUCTION (i.e. BUILDING, UTILITY CONNECTIONS, ETC.).
- 17. LOAM AND SEED ALL DISTURBED AREAS AND INSTALL ANY REQUIRED SEDIMENT AND EROSION CONTROL FACILITIES (i.e. RIP RAP, EROSION CONTROL BLANKETS, ETC.).
- 18. FINISH PAVING ALL ROADWAYS WITH 'FINISH' COURSE.
- 19. ALL ROADWAYS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 20. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 21. COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- 22. REMOVE TEMPORARY EROSION CONTROL MEASURES AFTER SEEDING AREAS HAVE BEEN 75%-85% ESTABLISHED AND SITE IMPROVEMENTS ARE COMPLETE. SMOOTH AND RE-VEGETATE ALL DISTURBED AREAS.
- 23. CLEAN SITE AND ALL DRAINAGE STRUCTURES, PIPES AND SUMPS OF ALL SILT AND DEBRIS.
- 24. INSTALL ALL PAINTED PAVEMENT MARKINGS AND SIGNAGE PER THE PLANS AND DETAILS.
- 25. ALL EROSION CONTROLS SHALL BE INSPECTED WEEKLY AND AFTER EVERY QUARTER-INCH OF RAINFALL
- 26. UPON COMPLETION OF CONSTRUCTION, IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY ANY RELEVANT PERMITTING AGENCIES THAT THE CONSTRUCTION HAS BEEN FINISHED IN A SATISFACTORY MANNER.

EROSION AND SEDIMENT CONTROL DETAILS

SULLIVAN SUBDIVISION Project:

112 HIGH STREET, STRATHAM, NH 03885 **ROBIN SULLIVAN** 8 WHITTAKER DRIVE, STRATHAM, NH 03885

SHEET 8 OF 8 **JBE PROJECT NO. 13070.1**

DRAWING No.

LAZ RMN PLB PO Box 219

-FENCING IS TO RUN WITH THE CONTOURS ACROSS A SLOPE

-MAXIMUM RECOMMENDED

CONTOUR LINES ___

600' RECOMMENDED MAXIMUM

-FLARE ENDS UPHILL TO PROVIDE

6. SILT FENCES SHALL BE REMOVED WHEN NO LONGER NEEDED AND THE SEDIMENT COLLECTED SHALL BE

1. SILT FENCES SHALL BE INSPECTED IMMEDIATELY AFTER EACH RAINFALL AND AT LEAST DAILY DURING

2. IF THE FABRIC ON A SILT FENCE SHOULD DECOMPOSE OR BECOME INEFFECTIVE DURING THE EXPECTED

3. SEDIMENT DEPOSITS SHOULD BE INSPECTED AFTER EVERY STORM EVENT. THE DEPOSITS SHOULD BE

4. SEDIMENT DEPOSITS THAT ARE REMOVED, OR LEFT IN PLACE AFTER THE FABRIC HAS BEEN REMOVED,

PROLONGED RAINFALL. ANY REPAIRS THAT ARE REQUIRED SHALL BE DONE IMMEDIATELY.

REMOVED WHEN THEY REACH APPROXIMATELY ONE HALF THE HEIGHT OF THE BARRIER.

SHALL BE GRADED TO CONFORM WITH THE EXISTING TOPOGRAPHY AND VEGETATED.

LIFE OF THE FENCE, THE FABRIC SHALL BE REPLACED PROMPTLY.

DISPOSED AS DIRECTED BY THE ENGINEER. THE AREA DISTURBED BY THE REMOVAL SHALL BE

STORAGE AREA

TRAPPING CAPABILITY AND SEDIMENT

- DISTURBED AREA

(UPHILL) -

SMOOTHED AND REVEGETATED.

MAINTENANCE:

UNCONTROLLED SLOPE LENGTH

Designed and Produced in NH

Civil Engineering Services 85 Portsmouth Ave. E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

603-772-4746 FAX: 603-772-0227 Owner of Record



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

DRAINAGE ANALYSIS SEDIMENT AND EROSION CONTROL PLAN

Prepared for:

Sullivan Subdivision Tax Map 19, Lot 68 High Street Stratham, NH 03885



June 29, 2017 Revised August 16, 2017 JBE Project No. 13070

EXECUTIVE SUMMARY

Robin Sullivan proposes to construct a 5-lot subdivision on a ±14.99-acre parcel of land located on the south side of High Street in Stratham, NH. A drainage analysis of the entire site and its offsite contributing watershed areas was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-construction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.23"), 10 Year – 24 Hour (4.91"), 25 Year – 24 Hour (6.24"), 50 Year – 24 Hour (7.48") and 100 Year – 24 Hour (8.97") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. A summary of the existing and proposed conditions peak rates of runoff is as follows:

COMPONENT	ANALYSIS	PEAK RATE OF RUNOFF (CUBIC FEET/SECOND)					
		2 Year	10 Year	25 Year	50 Year	100 Year	
Reach #1	Existing	10.13	25.04	38.37	51.43	67.97	
Analysis Point #1	Proposed	9.30	22.97	35.20	47.18	62.35	
Reach #2	Existing	4.93	14.19	22.75	31.29	41.99	
Analysis Point #2	Proposed	4.43	12.68	19.41	25.88	33.80	

The project site is located in the Rural Residential Zone. The subject parcel consists primarily of woodland and grass. The site is primarily undeveloped with the exception of an existing house in the western corner adjacent to Whittaker Drive. The existing topography is such that the existing conditions site analysis requires two (2) subcatchments. The site and contributing off-site runoff drains to two wetlands, one located in the southeast corner (Analysis Point #1) and one located on the eastern property line approximately 450' northeast of the southeast corner wetland (Analysis Point #2).

The proposed site development consists of the aforementioned 5-lot subdivision, featuring single-family dwellings. The construction of approximately 1,133 feet of roadway, driveways, and homes, in addition to site grading, divides the existing drainage basins into five (5) subcatchments. The runoff from these subcatchments has increased from that of the existing conditions due to the addition of the impervious buildings and paving. The runoff from the roadway will be directed via site grading and swales to a detention pond. Stormwater from the houses and driveways will be directed to drip edges. As shown in the above table, the proposed peak rates of stormwater runoff will be reduced from that of existing conditions for all analyzed storm events.

In addition, the potential for increased erosion and sedimentation is handled by way of erosion control blankets, vegetated treatment, and riprap inlet and outlet protection aprons. All land disturbed during construction will be stabilized within thirty days of groundbreaking, and existing wetlands and abutting property owners will suffer minimal adversity resultant of this development.

TABLE OF CONTENTS

Executive Summary

USGS	Ouadr	angle
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Enclosed:

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1.0	Rainfall Characteristics					
2.0	Ex	isting Conditions Analysis	Page 2			
3.0	Pro	oposed Conditions Analysis	Pages 3-4			
4.0	Co	nclusion	Page 5			
Appendix	I	Existing Conditions Analysis				
Appendix	Ш	2 Year - 24 Hour Summary 10 Year - 24 Hour Summary 25 Year - 24 Hour Complete 50 Year - 24 Hour Summary 100 Year - 24 Hour Complete Proposed Conditions Analysis 2 Year - 24 Hour Summary 10 Year - 24 Hour Summary 25 Year - 24 Hour Complete 50 Year - 24 Hour Complete 50 Year - 24 Hour Complete				
Appendix 2	III	Charts, Graphs, and Calculations				

Existing Conditions Watershed Plan Proposed Conditions Watershed Plan

1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same location. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (3.23"), 10 Year – 24 Hour (4.91"), 25 Year – 24 Hour (6.24"), 50 Year – 24 Hour (7.48") and 100 Year – 24 Hour (8.97") storm events.

As the table in the Executive Summary demonstrates, the proposed peak rates of runoff will be reduced from the existing conditions of the site, thereby minimizing any potential for a negative impact on abutting properties or infrastructure by allowing for better control of peak rates of stormwater runoff.

2.0 EXISTING CONDITIONS ANALYSIS

The subject parcel consists primarily of woodland and grass. The site is primarily undeveloped with the exception of an existing house in the western corner adjacent to Whittaker Drive. The topography of the site varies from flat to steep throughout the site, with few slopes exceeding 15%.

Classified through the use of Natural Resources Conservation Service's Web Soil Survey, the land of the site is composed of a variety of soil types. The in-situ soils are categorized into Hydrologic Soil Groups (HSG) B and C (see appendix for soil types and HSG designations).

The site and contributing off-site runoff drains to two wetlands, one located in the southeast corner (Analysis Point #1) and one located on the eastern property line approximately 450' northeast of the southeast corner wetland (Analysis Point #2).

3.0 PROPOSED CONDITIONS ANALYSIS

The proposed site development consists of the aforementioned 5-lot subdivision, featuring single-family dwellings. The construction of approximately 1,133 feet of roadway, driveways, and homes, in addition to site grading, divides the existing drainage basins into five (5) subcatchments. The runoff from these subcatchments has increased from that of the existing conditions due to the addition of the impervious buildings and paving.

The runoff from the roadway will be directed via site grading and swales to a detention pond. Stormwater from the houses and driveways will be directed to drip edges. As shown in the above table, the proposed peak rates of stormwater runoff will be reduced from that of existing conditions for all analyzed storm events.

4.0 CONCLUSION

This proposed site development located south of High Street in Stratham, NH will have minimal adverse effect on abutting infrastructures or properties by way of stormwater runoff or siltation. The post-construction peak rates of runoff for the site will be lower than the existing conditions for all analyzed storm events. Appropriate steps will be taken to eliminate erosion and sedimentation; these will be accomplished through the construction of a drainage system consisting of site grading, jute matting, vegetated swales, detention ponds, and riprap outlet protection aprons.

A site specific, terrain alteration permit (RSA 485:A-17) is not required for this site plan due to the area of disturbance being less than 100,000 square-feet.

Respectfully Submitted,

MD J. Kin

JONES & BEACH ENGINEERS, INC.

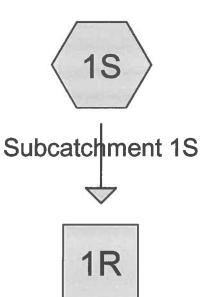
Michael Kerivan, P.E.

Project Engineer

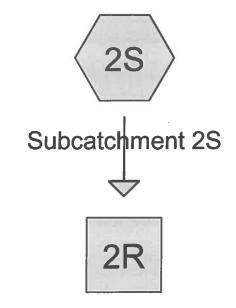
APPENDIX I

EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Summary 10 YEAR Complete 25 YEAR Summary 50 YEAR Complete 100 YEAR



Analysis Point #1



Analysis Point #2









Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
4.808	61	>75% Grass cover, Good, HSG B (1S, 2S)
8.430	74	>75% Grass cover, Good, HSG C (1S, 2S)
0.153	98	Paved roads w/curbs & sewers, HSG B (2S)
0.222	98	Paved roads w/curbs & sewers, HSG C (1S, 2S)
0.318	98	Roofs, HSG B (1S, 2S)
0.432	98	Roofs, HSG C (1S, 2S)
2.521	55	Woods, Good, HSG B (1S, 2S)
5.846	70	Woods, Good, HSG C (1S, 2S)
22.731	69	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
7.801	HSG B	1S, 2S
14.930	HSG C	1S, 2S
0.000	HSG D	
0.000	Other	
22.731		TOTAL AREA

Type III 24-hr 2-YR STORM Rainfall=3.23"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S

Runoff Area=579,886 sf 4.56% Impervious Runoff Depth>0.89" Flow Length=1,150' Tc=12.6 min CN=71 Runoff=10.13 cfs 0.991 af

Subcatchment 2S: Subcatchment 2S

Runoff Area=410,294 sf 5.51% Impervious Runoff Depth>0.70" Flow Length=904' Tc=14.1 min CN=67 Runoff=4.93 cfs 0.549 af

Reach 1R: Analysis Point #1

Inflow=10.13 cfs 0.991 af Outflow=10.13 cfs 0.991 af

Reach 2R: Analysis Point #2

Inflow=4.93 cfs 0.549 af Outflow=4.93 cfs 0.549 af

Total Runoff Area = 22.731 ac Runoff Volume = 1.540 af Average Runoff Depth = 0.81" 95.05% Pervious = 21.606 ac 4.95% Impervious = 1.126 ac

Type III 24-hr 10-YR STORM Rainfall=4.91"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S

Runoff Area=579,886 sf 4.56% Impervious Runoff Depth>2.04" Flow Length=1,150' Tc=12.6 min CN=71 Runoff=25.04 cfs 2.267 af

Subcatchment 2S: Subcatchment 2S

Runoff Area=410,294 sf 5.51% Impervious Runoff Depth>1.73" Flow Length=904' Tc=14.1 min CN=67 Runoff=14.19 cfs 1.362 af

Reach 1R: Analysis Point #1

Inflow=25.04 cfs 2.267 af Outflow=25.04 cfs 2.267 af

Reach 2R: Analysis Point #2

Inflow=14.19 cfs 1.362 af Outflow=14.19 cfs 1.362 af

Total Runoff Area = 22.731 ac Runoff Volume = 3.629 af Average Runoff Depth = 1.92" 95.05% Pervious = 21.606 ac 4.95% Impervious = 1.126 ac

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S

Runoff Area=579,886 sf 4.56% Impervious Runoff Depth>3.09"

Flow Length=1,150' Tc=12.6 min CN=71 Runoff=38.37 cfs 3.423 af

Subcatchment 2S: Subcatchment 2S

Runoff Area=410,294 sf 5.51% Impervious Runoff Depth>2.70"

Flow Length=904' Tc=14.1 min CN=67 Runoff=22.75 cfs 2.123 af

Reach 1R: Analysis Point #1

Inflow=38.37 cfs 3.423 af

Outflow=38.37 cfs 3.423 af

Reach 2R: Analysis Point #2

Inflow=22.75 cfs 2.123 af

Outflow=22.75 cfs 2.123 af

Total Runoff Area = 22.731 ac Runoff Volume = 5.546 af Average Runoff Depth = 2.93" 95.05% Pervious = 21.606 ac 4.95% Impervious = 1.126 ac HydroCAD® 10.00-20 s/n 03433 © 2017 HydroCAD Software Solutions LLC

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff

38.37 cfs @ 12.18 hrs, Volume=

3.423 af, Depth> 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

	Α	rea (sf)	CN	Description					
		3,413	98	98 Roofs, HSG B					
		15,248	98	Roofs, HSC	G C				
		7,767				& sewers, HSG C			
		96,134				ood, HSG B			
		90,072				ood, HSG C			
		33,890		Woods, Go	•				
_	1	33,362	70	Woods, Go	<u>od, HSG C</u>				
		79,886		Weighted A	_				
		53,458		95.44% Pe					
		26,428		4.56% Impe	ervious Are	a			
	т.	Lanadh	Clana	\/alaaih.	Consoitu	Description			
	Tc (min)	Length (foot)	Slope		Capacity	Description			
-	(min)	(feet)	(ft/ft)		(cfs)	Chart Flour			
	0.2	10	0.0200	0.87		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.23"			
	2.7	40	0.0800	0.25		Sheet Flow,			
	2.1	40	0.0000	0.25		Grass: Short n= 0.150 P2= 3.23"			
	2.3	155	0.0250	1.11		Shallow Concentrated Flow,			
	2.0	100	0.0200	,		Short Grass Pasture Kv= 7.0 fps			
	5.1	550	0.0650	1.78		Shallow Concentrated Flow,			
	• • • • • • • • • • • • • • • • • • • •		0.000			Short Grass Pasture Kv= 7.0 fps			
	2.3	395	0.0350	2.81		Shallow Concentrated Flow,			
				_		Grassed Waterway Kv= 15.0 fps			
_	12.6	1.150	Total						

Summary for Subcatchment 2S: Subcatchment 2S

Runoff

22.75 cfs @ 12.20 hrs, Volume=

2.123 af, Depth> 2.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

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A	rea (sf)	CN E	escription					
	10,444	98 F	98 Roofs, HSG B					
	3,571	98 F	Roofs, HSG	C				
	6,684	98 F	Paved road	s w/curbs &	& sewers, HSG B			
	1,907	98 F	Paved road	s w/curbs &	& sewers, HSG C			
	13,323			•	ood, HSG B			
	77,154				ood, HSG C			
	75,937			od, HSG B				
1	21,274	70 V	Voods, Go	od, HSG C				
4	10,294	67 V	Veighted A	verage				
3	87,688	9	4.49% Per	vious Area				
	22,606	5	.51% Impe	rvious Are	a			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
0.2	13	0.0200	0.92		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.23"			
3.3	37	0.0400	0.18		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.23"			
1.4	120	0.0400	1.40		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
2.1	125	0.0400	1.00		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
2.2	184	0.0400	1.40		Shallow Concentrated Flow,			
			4.40		Short Grass Pasture Kv= 7.0 fps			
4.9	425	0.0850	1.46		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
14.1	904	Total						

Summary for Reach 1R: Analysis Point #1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 13.312 ac, 4.56% Impervious, Inflow Depth > 3.09" for 25-YR STORM event

Inflow = 38.37 cfs @ 12.18 hrs, Volume= 3.423 af

Outflow = 38.37 cfs @ 12.18 hrs, Volume= 3.423 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach 2R: Analysis Point #2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 9.419 ac, 5.51% Impervious, Inflow Depth > 2.70" for 25-YR STORM event

Inflow = 22.75 cfs @ 12.20 hrs, Volume= 2.123 af

Outflow = 22.75 cfs @ 12.20 hrs, Volume= 2.123 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 50-YR STORM Rainfall=7.48"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S

Runoff Area=579,886 sf 4.56% Impervious Runoff Depth>4.12"

Flow Length=1,150' Tc=12.6 min CN=71 Runoff=51.43 cfs 4.572 af

Subcatchment 2S: Subcatchment 2S

Runoff Area=410,294 sf 5.51% Impervious Runoff Depth>3.68"

Flow Length=904' Tc=14.1 min CN=67 Runoff=31.29 cfs 2.891 af

Reach 1R: Analysis Point #1

Inflow=51.43 cfs 4.572 af

Outflow=51.43 cfs 4.572 af

Reach 2R: Analysis Point #2

Inflow=31.29 cfs 2.891 af Outflow=31.29 cfs 2.891 af

Total Runoff Area = 22.731 ac Runoff Volume = 7.464 af Average Runoff Depth = 3.94" 95.05% Pervious = 21.606 ac 4.95% Impervious = 1.126 ac

Type III 24-hr 100-YR STORM Rainfall=8.97"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S

Runoff Area=579,886 sf 4.56% Impervious Runoff Depth>5.42" Flow Length=1,150' Tc=12.6 min CN=71 Runoff=67.97 cfs 6.013 af

Subcatchment 2S: Subcatchment 2S

Runoff Area=410,294 sf 5.51% Impervious Runoff Depth>4.93" Flow Length=904' Tc=14.1 min CN=67 Runoff=41.99 cfs 3.866 af

Reach 1R: Analysis Point #1

Inflow=67.97 cfs 6.013 af Outflow=67.97 cfs 6.013 af

Reach 2R: Analysis Point #2

Inflow=41.99 cfs 3.866 af Outflow=41.99 cfs 3.866 af

Total Runoff Area = 22.731 ac Runoff Volume = 9.879 af Average Runoff Depth = 5.22" 95.05% Pervious = 21.606 ac 4.95% Impervious = 1.126 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff

67.97 cfs @ 12.17 hrs, Volume=

6.013 af, Depth> 5.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

	Area (sf)	CN	Description					
	3,413	98	98 Roofs, HSG B					
	15,248	98	Roofs, HSC	3 C				
	7,767	98	Paved road	ls w/curbs &	& sewers, HSG C			
	96,134	61	>75% Gras	s cover, Go	ood, HSG B			
	290,072				ood, HSG C			
	33,890		Woods, Go	,				
	133,362		Noods, Go	<u>od, HSG C</u>				
	579,886		Neighted A					
	553,458		95.44% Pei					
	26,428	4	4.56% Impe	ervious Are	a			
т.		01	17.1-26	0 "	D			
To	_	Slope	-		Description			
(min		(ft/ft)		(cfs)				
0.2	2 10	0.0200	0.87		Sheet Flow,			
2.7	7 40	0.0800	0.05		Smooth surfaces n= 0.011 P2= 3.23"			
2.1	40	0.0000	0.25		Sheet Flow, Grass: Short n= 0.150 P2= 3.23"			
2.3	155	0.0250	1.11		Shallow Concentrated Flow,			
2.0	, 155	0.0230	1.11		Short Grass Pasture Kv= 7.0 fps			
5.1	550	0.0650	1.78		Shallow Concentrated Flow,			
	000	0.0000	0		Short Grass Pasture Kv= 7.0 fps			
2.3	395	0.0350	2.81		Shallow Concentrated Flow,			
		,			Grassed Waterway Kv= 15.0 fps			
12.6	1,150	Total	_					

1,150 lotal

Summary for Subcatchment 2S: Subcatchment 2S

Runoff

41.99 cfs @ 12.20 hrs, Volume=

3.866 af, Depth> 4.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

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A	rea (sf)	CN I	Description					
	10,444	98 I	98 Roofs, HSG B					
	3,571	98	Roofs, HSC	e C				
	6,684	98	Paved road	s w/curbs &	& sewers, HSG B			
	1,907				& sewers, HSG C			
	13,323	61 >	>75% Gras	s cover, Go	ood, HSG B			
	77,154		>75% Gras	s cover, Go	ood, HSG C			
	75,937		Noods, Go					
1	21,274	70 \	<u> Voods, Go</u>	<u>od, HSG C</u>		_		
4	110,294	67 \	Neighted A	verage				
3	87,688	9	94.49% Per	vious Area				
	22,606	5	5.51% Impe	ervious Are	a			
Тс	Length	Slope		Capacity	Description			
(min)	(feet)	(ft/ft)		(cfs)				
0.2	13	0.0200	0.92		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.23"			
3.3	37	0.0400	0.18		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.23"			
1.4	120	0.0400	1.40		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
2.1	125	0.0400	1.00		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
2.2	184	0.0400	1.40		Shallow Concentrated Flow,			
4.0	40=	0.0050	4 45		Short Grass Pasture Kv= 7.0 fps			
4.9	425	0.0850	1.46		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps	_		
14.1	904	Total						

Summary for Reach 1R: Analysis Point #1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 13.312 ac, 4.56% Impervious, Inflow Depth > 5.42" for 100-YR STORM event

Inflow = 67.97 cfs @ 12.17 hrs, Volume= 6.013 af

Outflow = 67.97 cfs @ 12.17 hrs, Volume= 6.013 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach 2R: Analysis Point #2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 9.419 ac, 5.51% Impervious, Inflow Depth > 4.93" for 100-YR STORM event

Inflow = 41.99 cfs @ 12.20 hrs, Volume= 3.866 af

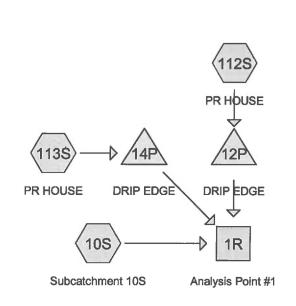
Outflow = 41.99 cfs @ 12.20 hrs, Volume= 3.866 af, Atten= 0%, Lag= 0.0 min

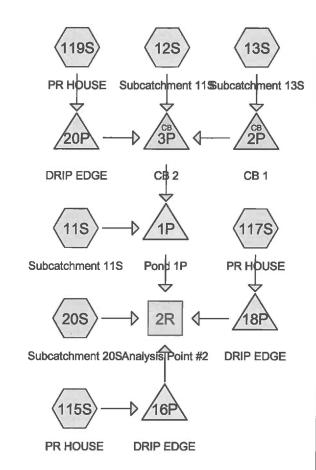
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

APPENDIX II

PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Summary 10 YEAR Complete 25 YEAR Summary 50 YEAR Complete 100 YEAR













Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
5.588	61	>75% Grass cover, Good, HSG B (10S, 11S, 12S, 13S, 20S)
9.151	74	>75% Grass cover, Good, HSG C (10S, 11S, 12S, 13S, 20S)
0.057	98	Paved parking, HSG C (112S, 113S, 115S, 117S, 119S)
0.379	98	Paved roads w/curbs & sewers, HSG B (11S, 12S, 13S, 20S)
0.518	98	Paved roads w/curbs & sewers, HSG C (10S, 11S, 12S, 13S, 20S)
0.281	98	Roofs, HSG B (10S, 12S, 20S)
0.699	98	Roofs, HSG C (10S, 20S, 112S, 113S, 115S, 117S, 119S)
1.553	55	Woods, Good, HSG B (10S, 20S)
4.504	70	Woods, Good, HSG C (10S, 11S, 12S, 20S)
22.731	71	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
7.801	HSG B	10S, 11S, 12S, 13S, 20S
14.930	HSG C	10S, 11S, 12S, 13S, 20S, 112S, 113S, 115S, 117S, 119S
0.000	HSG D	
0.000	Other	
22.731		TOTAL AREA

Type III 24-hr 2-YR STORM Rainfall=3.23"

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Outflow=0.00 cfs 0.000 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

r todon rodding k	by Dyll Otol-III	a method - i om	a routing by b	yri-otor-	ina metrioa	
Subcatchment 10S: Subcate		Runoff Area=53 ow Length=1,150'				
Subcatchment 11S: Subcatch		Runoff Area=60 Flow Length=611'				
Subcatchment 12S: Subcatc	hment 11S	Runoff Area=127 Flow Length=736				
Subcatchment 13S: Subcatch	hment 13S	Runoff Area=14			ious Runoff Runoff=0.54	
Subcatchment 20S: Subcatc	hment 20S	Runoff Area=24 Flow Length=627				
Subcatchment 112S: PR HO	USE	Runoff Area=3,0			vious Runoff Runoff=0.25	
Subcatchment 113S: PR HO	USE	Runoff Area=3,0			ious Runoff Runoff=0.25	
Subcatchment 115S: PR HO	USE	Runoff Area=3,0			rious Runoff Runoff=0.25	
Subcatchment 117S: PR HO	USE	Runoff Area=3,0			rious Runoff Runoff=0.25	
Subcatchment 119S: PR HO	USE	Runoff Area=3,0			ious Runoff Runoff=0.25	
Reach 1R: Analysis Point #1				(Inflow=9.30 Outflow=9.30	cfs 0.909 af cfs 0.909 af
Reach 2R: Analysis Point #2				(Inflow=4.43 Outflow=4.43	cfs 0.692 af cfs 0.692 af
Pond 1P: Pond 1P	12.0" Round	Peak Elev=80 Culvert n=0.013 L).78' Storage= .=110.0' S=0.(
Pond 2P: CB 1	15.0" Round	Culvert n=0.013			Inflow=0.54 Outflow=0.54	
Pond 3P: CB 2	24.0" Round	Culvert n=0.013			Inflow=2.82 Outflow=2.82	
Pond 12P: DRIP EDGE		Peak Elev=	88.16' Storage	=749 cf	Inflow=0.25	cfs 0.017 af

Type III 24-hr 2-YR STORM Rainfall=3.23"

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Pond 14P: DRIP EDGE

Peak Elev=88.16' Storage=749 cf Inflow=0.25 cfs 0.017 af

Outflow=0.00 cfs 0.000 af

Pond 16P: DRIP EDGE

Peak Elev=88.16' Storage=749 cf Inflow=0.25 cfs 0.017 af

Outflow=0.00 cfs 0.000 af

Pond 18P: DRIP EDGE

Peak Elev=88.16' Storage=749 cf Inflow=0.25 cfs 0.017 af

Outflow=0.00 cfs 0.000 af

Pond 20P: DRIP EDGE

Peak Elev=88.16' Storage=749 cf Inflow=0.25 cfs 0.017 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 22.731 ac Runoff Volume = 1.706 af Average Runoff Depth = 0.90" 91.49% Pervious = 20.797 ac 8.51% Impervious = 1.935 ac

Type III 24-hr 10-YR STORM Rainfall=4.91"

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Outflow=0.00 cfs 0.000 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method

Reach routing I	by Dyn-Stor-Ind	d method - Pond routing by Dyn-Stor-Ind method
Subcatchment 10S: Subcate		Runoff Area=531,948 sf 4.81% Impervious Runoff Depth>2.04" w Length=1,150' Tc=12.6 min CN=71 Runoff=22.97 cfs 2.079 af
Subcatchment 11S: Subcate		Runoff Area=60,477 sf 15.00% Impervious Runoff Depth>2.54" Flow Length=611' Tc=11.2 min CN=77 Runoff=3.46 cfs 0.294 af
Subcatchment 12S: Subcate	chment 11S	Runoff Area=127,930 sf 12.65% Impervious Runoff Depth>1.97" Flow Length=736' Tc=8.5 min CN=70 Runoff=5.95 cfs 0.481 af
Subcatchment 13S: Subcato	chment 13S	Runoff Area=14,396 sf 43.66% Impervious Runoff Depth>2.81" Tc=6.0 min CN=80 Runoff=1.07 cfs 0.077 af
Subcatchment 20S: Subcato	chment 20S	Runoff Area=240,429 sf 5.06% Impervious Runoff Depth>1.74" Flow Length=627' Tc=9.5 min CN=67 Runoff=9.48 cfs 0.799 af
Subcatchment 112S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.67" Tc=0.0 min CN=98 Runoff=0.38 cfs 0.027 af
Subcatchment 113S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.67" Tc=0.0 min CN=98 Runoff=0.38 cfs 0.027 af
Subcatchment 115S: PR HO	USE	Runoff Area=3,000 sf 100:00% Impervious Runoff Depth>4.67" Tc=0.0 min CN=98 Runoff=0.38 cfs 0.027 af
Subcatchment 117S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.67" Tc=0.0 min CN=98 Runoff=0.38 cfs 0.027 af
Subcatchment 119S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.67" Tc=0.0 min CN=98 Runoff=0.38 cfs 0.027 af
Reach 1R: Analysis Point #1		Inflow=22.97 cfs 2.079 af Outflow=22.97 cfs 2.079 af
Reach 2R: Analysis Point #2		Inflow=12.68 cfs 1.627 af Outflow=12.68 cfs 1.627 af
Pond 1P: Pond 1P	12.0" Round (Peak Elev=81.68' Storage=10,075 cf Inflow=10.26 cfs 0.853 af Culvert n=0.013 L=110.0' S=0.0655 '/' Outflow=4.11 cfs 0.828 af
Pond 2P: CB 1	15.0" Round	Peak Elev=86.55' Inflow=1.07 cfs 0.077 afd Culvert n=0.013 L=50.0' S=0.0050 '/' Outflow=1.07 cfs 0.077 afd
Pond 3P: CB 2	24.0" Round	Peak Elev=86.51' Inflow=7.01 cfs 0.559 af Culvert n=0.013 L=52.0' S=0.0048'/' Outflow=7.01 cfs 0.559 af
Pond 12P: DRIP EDGE		Peak Elev=89.37' Storage=1,168 cf Inflow=0.38 cfs 0.027 af

Type III 24-hr 10-YR STORM Rainfall=4.91"

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Pond 14P: DRIP EDGE

Peak Elev=89.37' Storage=1,168 cf Inflow=0.38 cfs 0.027 af

Outflow=0.00 cfs 0.000 af

Pond 16P: DRIP EDGE

Peak Elev=89.37' Storage=1,168 cf Inflow=0.38 cfs 0.027 af

Outflow=0.00 cfs 0.000 af

Pond 18P: DRIP EDGE

Peak Elev=89.37' Storage=1,168 cf Inflow=0.38 cfs 0.027 af

Outflow=0.00 cfs 0.000 af

Pond 20P: DRIP EDGE

Peak Elev=89.37' Storage=1,168 cf Inflow=0.38 cfs 0.027 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 22.731 ac Runoff Volume = 3.865 af Average Runoff Depth = 2.04" 91.49% Pervious = 20.797 ac 8.51% Impervious = 1.935 ac

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Outflow=0.01 cfs 0.003 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Reach routing by Dyn-St	tor-ind method - Pond routing by Dyn-Stor-ind method
Subcatchment 10S: Subcatchment 1	OS Runoff Area=531,948 sf 4.81% Impervious Runoff Depth>3.09" Flow Length=1,150' Tc=12.6 min CN=71 Runoff=35.20 cfs 3.140 af
Subcatchment 11S: Subcatchment 1	Runoff Area=60,477 sf 15.00% Impervious Runoff Depth>3.68" Flow Length=611' Tc=11.2 min CN=77 Runoff=5.02 cfs 0.426 af
Subcatchment 12S: Subcatchment 1	Runoff Area=127,930 sf 12.65% Impervious Runoff Depth>2.99" Flow Length=736' Tc=8.5 min CN=70 Runoff=9.29 cfs 0.732 af
Subcatchment 13S: Subcatchment 13	Runoff Area=14,396 sf 43.66% Impervious Runoff Depth>4.00" Tc=6.0 min CN=80 Runoff=1.51 cfs 0.110 af
Subcatchment 20S: Subcatchment 20	Runoff Area=240,429 sf 5.06% Impervious Runoff Depth>2.71" Flow Length=627' Tc=9.5 min CN=67 Runoff=15.17 cfs 1.245 af
Subcatchment 112S: PR HOUSE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>6.00" Tc=0.0 min CN=98 Runoff=0.48 cfs 0.034 af
Subcatchment 113S: PR HOUSE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>6.00" Tc=0.0 min CN=98 Runoff=0.48 cfs 0.034 af
Subcatchment 115S: PR HOUSE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>6.00" Tc=0.0 min CN=98 Runoff=0.48 cfs 0.034 af
Subcatchment 117S: PR HOUSE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>6.00" Tc=0.0 min CN=98 Runoff=0.48 cfs 0.034 af
Subcatchment 119S: PR HOUSE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>6.00" Tc=0.0 min CN=98 Runoff=0.48 cfs 0.034 af
Reach 1R: Analysis Point #1	Inflow=35.20 cfs 3.145 af Outflow=35.20 cfs 3.145 af
Reach 2R: Analysis Point #2	Inflow=19.41 cfs 2.492 af Outflow=19.41 cfs 2.492 af
Pond 1P: Pond 1P 12.0" Ro	Peak Elev=82.51' Storage=15,979 cf Inflow=15.40 cfs 1.271 afound Culvert n=0.013 L=110.0' S=0.0655 '/' Outflow=5.36 cfs 1.242 af
Pond 2P: CB 1	Peak Elev=87.03' Inflow=1.51 cfs 0.110 af Round Culvert n=0.013 L=50.0' S=0.0050 '/' Outflow=1.51 cfs 0.110 af
Pond 3P: CB 2	Peak Elev=86.97' Inflow=10.72 cfs 0.845 af bund Culvert n=0.013 L=52.0' S=0.0048'/' Outflow=10.72 cfs 0.845 af
Pond 12P: DRIP EDGE	Peak Elev=90.00' Storage=1,391 cf Inflow=0.48 cfs 0.034 af

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Pond 14P: DRIP EDGE Peak Elev=90.00'

Peak Elev=90.00' Storage=1,391 cf Inflow=0.48 cfs 0.034 af

Outflow=0.01 cfs 0.003 af

Pond 16P: DRIP EDGE Peak Elev=90.00' Storage=1,391 cf Inflow=0.48 cfs 0.034 af

Outflow=0.01 cfs 0.003 af

Pond 18P: DRIP EDGE Peak Elev=90.00' Storage=1,391 cf Inflow=0.48 cfs 0.034 af

Outflow=0.01 cfs 0.003 af

Pond 20P: DRIP EDGE Peak Elev=90.00' Storage=1,391 cf Inflow=0.48 cfs 0.034 af

Outflow=0.01 cfs 0.003 af

Total Runoff Area = 22.731 ac Runoff Volume = 5.826 af Average Runoff Depth = 3.08" 91.49% Pervious = 20.797 ac 8.51% Impervious = 1.935 ac

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Summary for Subcatchment 10S: Subcatchment 10S

Runoff

35.20 cfs @ 12.18 hrs, Volume=

3.140 af, Depth> 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

	Α	rea (sf)	CN [Description				
		3,413	98 F	98 Roofs, HSG B				
		14,383	98 F	Roofs, HSG	e C			
		7,767	98 F	Paved road	s w/curbs &	& sewers, HSG C		
		98,769				ood, HSG B		
		60,481				ood, HSG C		
		30,102			od, HSG B			
_		17,033			<u>od, HSG C</u>	The state of the s	_	
		31,948		Veighted A	_			
		06,385			vious Area			
		25,563	4	I.81% Impe	ervious Area	a		
	т.	Lasastla	01	V-19-	0	Description		
	Tc	Length	Slope	Velocity	Capacity	Description		
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Oh a st Flore	-	
	0.2	10	0.0200	0.87		Sheet Flow,		
	2.7	40	0.0800	0.25		Smooth surfaces n= 0.011 P2= 3.23" Sheet Flow,		
	2.1	40	0.0000	0.25		Grass: Short n= 0.150 P2= 3.23"		
	2.3	155	0.0250	1.11		Shallow Concentrated Flow.		
	2.0	100	0.0200			Short Grass Pasture Kv= 7.0 fps		
	5.1	550	0.0650	1.78		Shallow Concentrated Flow,		
	• • • •					Short Grass Pasture Kv= 7.0 fps		
	2.3	395	0.0350	2.81		Shallow Concentrated Flow,		
						Grassed Waterway Kv= 15.0 fps		
_	12.6	1.150	Total				-	

Summary for Subcatchment 11S: Subcatchment 11S

Runoff

5.02 cfs @ 12.16 hrs, Volume=

0.426 af, Depth> 3.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

Area (sf)	CN	Description
3,900	98	Paved roads w/curbs & sewers, HSG B
5,174	98	Paved roads w/curbs & sewers, HSG C
1,866	61	>75% Grass cover, Good, HSG B
42,233	74	>75% Grass cover, Good, HSG C
7,304	70	Woods, Good, HSG C
60,477	77	Weighted Average
51,403		85.00% Pervious Area
9,074		15.00% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	5.6	50	0.0200	0.15		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.23"
	5.3	495	0.0500	1.57		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.2	36	0.0200	2.87		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	0.1	30	0.3300	4.02		Shallow Concentrated Flow,
_						Short Grass Pasture Kv= 7.0 fps
	11.2	611	Total			

Summary for Subcatchment 12S: Subcatchment 11S

Runoff = 9.29 cfs @ 12.12 hrs, Volume=

0.732 af, Depth> 2.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

	Area (sf)	(sf) CN	Description		
	5,122	22 98	Roofs, HSC	B	
	6,235	235 98	Paved road	s w/curbs &	& sewers, HSG B
	4,824		Paved road	s w/curbs &	& sewers, HSG C
	63,142		>75% Gras	s cover, Go	ood, HSG B
	41,943				ood, HSG C
	6,664		Woods, Go	<u>od, HSG C</u>	
	127,930		Weighted A		
•	111,749		87.35% Per		
	16,181	81	12.65% Imp	pervious Ar	ea
_					
Tc					Description
<u>(min)</u>	(feet)			(cfs)	
0.2	13	13 0.020	0.92		Sheet Flow,
0.0	0.7	07 0040			Smooth surfaces n= 0.011 P2= 3.23"
3.3	37	37 0.040	0.18		Sheet Flow,
0.0	400	100 0.010	1 00		
2.0	120	120 0.040	J 1.00		
2.5	211	211 0 040	1 40		
2.5	211	211 0.040	1.40		
0.5	355	355 0.032	1220	172 20	
0.5	555	0.002	12.30	173.39	
9.5	726	726 Total			11- 0.022 Earth, Clean & Straight
2.0 2.5 0.5	120 211 355 736	211 0.040 355 0.032	1.40	173.39	Grass: Short n= 0.150 P2= 3.23" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Trap/Vee/Rect Channel Flow, Bot.W=1.00' D=2.00' Z= 3.0 '/' Top.W=13.00' n= 0.022 Earth, clean & straight

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Summary for Subcatchment 13S: Subcatchment 13S

Runoff

=

1.51 cfs @ 12.09 hrs, Volume=

0.110 af, Depth> 4.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

A	rea (sf)	CN	Description					
	3,684	98	Paved road	s w/curbs &	& sewers, HSG B			
	2,602	98	Paved road	s w/curbs &	& sewers, HSG C			
	4,639	61	>75% Gras	s cover, Go	Good, HSG B			
	3,471	74	>75% Gras	s cover, Go	Good, HSG C			
	14,396	80	Weighted A	verage				
	8,110		56.34% Pervious Area					
	6,286		43.66% Impervious Area					
Tc	Length	Slope		Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 20S: Subcatchment 20S

Runoff

15.17 cfs @ 12.14 hrs, Volume=

1.245 af, Depth> 2.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

Area (sf)	CN	Description			
3,685	98	Roofs, HSG B			
3,571	98	Roofs, HSG C			
2,703	98	Paved roads w/curbs & sewers, HSG B			
2,218	98	Paved roads w/curbs & sewers, HSG C			
75,016	61	>75% Grass cover, Good, HSG B			
50,500	74	>75% Grass cover, Good, HSG C			
37,550	55	Woods, Good, HSG B			
65,186	70	Woods, Good, HSG C			
240,429	67	Weighted Average			
228,252		94.94% Pervious Area			
12,177		5.06% Impervious Area			

Type III 24-hr 25-YR STORM Rainfall=6.24"

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_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.3	17	0.0200	0.97		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.23"
	2.1	33	0.1000	0.26		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.23"
	2.5	165	0.0500	1.12		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	4.6	412	0.0900	1.50		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	9.5	627	Total			

Summary for Subcatchment 112S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.48 cfs @ 12.00 hrs, Volume=

0.034 af, Depth> 6.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6,24"

Area (sf)	CN	Description
2,500	98	Roofs, HSG C
500	98	Paved parking, HSG C
3,000 3,000	98	Weighted Average 100.00% Impervious Area

Summary for Subcatchment 113S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.48 cfs @ 12.00 hrs, Volume=

0.034 af, Depth> 6.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs. dt= 0.05 hrs. Type III 24-hr 25-YR STORM Rainfall=6.24"

Area (sf)	CN	Description
2,500	98	Roofs, HSG C
 500	98	Paved parking, HSG C
3,000	98	Weighted Average
3,000		100.00% Impervious Area

Summary for Subcatchment 115S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.48 cfs @ 12.00 hrs, Volume=

0.034 af, Depth> 6.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Area_(sf)	CN	Description		
2,500	98	Roofs, HSG C		
500	98	Paved parking, HSG C		
3,000 3,000	98	Weighted Average 100.00% Impervious Area		

Summary for Subcatchment 117S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.48 cfs @ 12.00 hrs, Volume=

0.034 af, Depth> 6.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

Area (sf)	CN	Description
2,500	98	Roofs, HSG C
500	98	Paved parking, HSG C
3,000 3,000	98	Weighted Average 100.00% Impervious Area

Summary for Subcatchment 119S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.48 cfs @ 12.00 hrs, Volume=

0.034 af, Depth> 6.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR STORM Rainfall=6.24"

Area (sf)	CN	Description	
2,500	98	Roofs, HSG C	
 500	_ 98	Paved parking, HSG C	
3,000	98	Weighted Average	
3,000		100.00% Impervious Area	

Summary for Reach 1R: Analysis Point #1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

12.350 ac, 5.87% Impervious, Inflow Depth > 3.06" for 25-YR STORM event

Inflow Outflow 35.20 cfs @ 12.18 hrs, Volume=

35.20 cfs @ 12.18 hrs, Volume=

3.145 af

3.145 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs. dt= 0.05 hrs.

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Summary for Reach 2R: Analysis Point #2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.382 ac, 11.66% Impervious, Inflow Depth > 2.88" for 25-YR STORM event

Inflow = 19.41 cfs @ 12.15 hrs, Volume= 2.492 af

Outflow = 19.41 cfs @ 12.15 hrs, Volume= 2.492 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1P: Pond 1P

Inflow Area = 4.725 ac, 16.78% Impervious, Inflow Depth > 3.23" for 25-YR STORM event

Inflow = 15.40 cfs @ 12.13 hrs, Volume= 1.271 af

Outflow = 5.36 cfs @ 12.49 hrs, Volume= 1.242 af, Atten= 65%, Lag= 21.7 min

Primary = 5.36 cfs @ 12.49 hrs, Volume= 1.242 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 82.51' @ 12.49 hrs Surf.Area= 7,538 sf Storage= 15,979 cf

Plug-Flow detention time= 48.9 min calculated for 1.242 af (98% of inflow)

Center-of-Mass det. time= 35.8 min (867.4 - 831.5)

#1	80.00'	3	7,994 cf	Custom Stage Dat	a (Irregular) Listed	below (Recald
Elevation (feet)		Area	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
80.00	5	5,262	277.0	0	0	5,262
82.00	7	7,037	314.7	12,256	12,256	7,133
84.00	9	9,096	357.0	16,089	28,345	9,492
85.00	10),213	377.4	9,649	37,994	10,739

#1 Primary 80.00' 12.0" Round Culvert

L= 110.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 80.00' / 72.80' S= 0.0655 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=5.36 cfs @ 12.49 hrs HW=82.51' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 5.36 cfs @ 6.83 fps)

Summary for Pond 2P: CB 1

Inflow Area = 0.330 ac, 43.66% Impervious, Inflow Depth > 4.00" for 25-YR STORM event

Inflow = 1.51 cfs @ 12.09 hrs, Volume= 0.110 af

Outflow = 1.51 cfs @ 12.09 hrs, Volume= 0.110 af, Atten= 0%, Lag= 0.0 min

Primary = 1.51 cfs @ 12.09 hrs. Volume= 0.110 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Peak Elev= 87.03' @ 12.16 hrs

Flood Elev= 89.80'

Device Routing Invert Outlet Devices

#1 Primary

85.55'

15.0" Round Culvert

L= 50.0' CPP, projecting, no headwall, Ke= 0.900

Inlet / Outlet Invert= 85.55' / 85.30' S= 0.0050 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=86.72' TW=86.90' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 3P: CB 2

[80] Warning: Exceeded Pond 2P by 0.18' @ 12.05 hrs (1.77 cfs 0.017 af)

Inflow Area = 3.336 ac, 17.52% Impervious, Inflow Depth > 3.04" for 25-YR STORM event

Inflow = 10.72 cfs @ 12.12 hrs, Volume= 0.845 af

Outflow = 10.72 cfs @ 12.12 hrs, Volume= 0.845 af, Atten= 0%, Lag= 0.0 min

Primary = 10.72 cfs @ 12.12 hrs, Volume= 0.845 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs. dt= 0.05 hrs.

Peak Elev= 86.97' @ 12.12 hrs

Flood Elev= 89.80'

Device Routing Invert Outlet Devices

#1 Primary

85.05'

24.0" Round Culvert

L= 52.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 85.05' / 84.80' S= 0.0048 '/' Cc= 0.900
n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=10.41 cfs @ 12.12 hrs HW=86.94' TW=81.59' (Dynamic Tailwater) 1=Culvert (Barrel Controls 10.41 cfs @ 4.39 fps)

Summary for Pond 12P: DRIP EDGE

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 6.00" for 25-YR STORM event

Inflow = 0.48 cfs @ 12.00 hrs, Volume= 0.034 af

Outflow = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af, Atten= 98%, Lag= 372.7 min

Primary = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.00' @ 18.20 hrs Surf.Area= 864 sf Storage= 1,391 cf

Plug-Flow detention time= 940.6 min calculated for 0.003 af (7% of inflow) Center-of-Mass det. time= 507.6 min (1,246.6 - 739.0)

Volume	Invert	Avail.Storage	Storage Description
#1	85.99'	1,823 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
85.99	864	0.0	0	0
86.00	864	40.0	3	3
89.99	864	40.0	1,379	1,382
90.00	864	100.0	9	1,391
90.50	864	100.0	432	1,823

Primary OutFlow Max=0.01 cfs @ 18.21 hrs HW=90.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.06 fps)

Summary for Pond 14P: DRIP EDGE

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 6.00" for 25-YR STORM event 0.48 cfs @ 12.00 hrs, Volume= 0.034 af

Outflow = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af, Atten= 98%, Lag= 372.7 min

Primary = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.00' @ 18.20 hrs Surf.Area= 864 sf Storage= 1,391 cf

Plug-Flow detention time= 940.6 min calculated for 0.003 af (7% of inflow)

Center-of-Mass det. time= 507.6 min (1,246.6 - 739.0)

Volume	Inv	<u>ert Ava</u>	il.Storage	Storage Descrip	tion	
#1	85.	99'	1,823 cf	Custom Stage I	Data (Prismatic) Lis	sted below (Recalc)
Flavoria		0	17-2-1-			
Elevation		Surf.Area	Voids	Inc.Store	Cum.Store	
(fee	<u>et) </u>	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1,391	
90.5	50	864	100.0	432	1,823	
Device	Routing	<u>In</u>	<u>vert Out</u>	et Devices		
#1	Primary	90	Hea			ed Rectangular Weir 1.20 1.40 1.60 1.80 2.00

Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31

Primary OutFlow Max=0.01 cfs @ 18.21 hrs HW=90.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.06 fps)

3.30 3.31 3.32

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Summary for Pond 16P: DRIP EDGE

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 6.00" for 25-YR STORM event

Inflow = 0.48 cfs @ 12.00 hrs, Volume= 0.034 af

Outflow = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af, Atten= 98%, Lag= 372.7 min

Primary = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.00' @ 18.20 hrs Surf.Area= 864 sf Storage= 1,391 cf

Plug-Flow detention time= 940.6 min calculated for 0.003 af (7% of inflow)

Invest A 9.04 Ot B 1.0

Center-of-Mass det. time= 507.6 min (1,246.6 - 739.0)

Volume	Inv	<u>rert Ava</u>	il.Storage	Storage Descri	ption	
#1	85.	99'	1,823 cf	Custom Stage	Data (Prismatic)	Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1,391	
90.5	50	864	100.0	432	1,823	
Device	Routing	In	vert Out	tlet Devices		
#1	Primary	90	.00' 230	0.0' long x 1.0' br	eadth Broad-Cres	sted Rectangular Weir
			Hea	ad (feet) 0.20 0.4	10 0.60 0.80 1.00	0 1.20 1.40 1.60 1.80 2.00
			2.5	0 3.00		
			Coe	ef. (English) 2.69	2.72 2.75 2.85	2.98 3.08 3.20 3.28 3.31
			3.3	0 3.31 3.32		

Primary OutFlow Max=0.01 cfs @ 18.21 hrs HW=90.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.06 fps)

Summary for Pond 18P: DRIP EDGE

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 6.00" for 25-YR STORM event

Inflow = 0.48 cfs @ 12.00 hrs, Volume= 0.034 af

Outflow = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af, Atten= 98%, Lag= 372.7 min

Primary = 0.01 cfs @ 18.21 hrs, Volume= 0.003 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.00' @ 18.20 hrs Surf.Area= 864 sf Storage= 1,391 cf

Plug-Flow detention time= 940.6 min calculated for 0.003 af (7% of inflow)

Center-of-Mass det. time= 507.6 min (1,246.6 - 739.0)

<u>Volume</u>	Invert	Avail.Storage	Storage Description
#1	85.99'	1,823 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Type III 24-hr 25-YR STORM Rainfall=6.24"

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
85.99	864	0.0	0	0
86.00	864	40.0	3	3
89.99	864	40.0	1,379	1,382
90.00	864	100.0	9	1,391
90.50	864	100.0	432	1,823
				,

Device	Routing	Invert	Outlet Devices
#1	Primary	90.00'	230.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Primary OutFlow Max=0.01 cfs @ 18.21 hrs HW=90.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.06 fps)

Summary for Pond 20P: DRIP EDGE

Inflow Area =	0.069 ac,100.00% Impervious, Inflow D	Depth > 6.00" for 25-YR STORM event
Inflow =	0.48 cfs @ 12.00 hrs, Volume=	0.034 af
Outflow =	0.01 cfs @ 18.21 hrs, Volume=	0.003 af, Atten= 98%, Lag= 372.7 min
Primary =	0.01 cfs @ 18.21 hrs, Volume=	0.003 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.00' @ 18.20 hrs Surf.Area= 864 sf Storage= 1,391 cf

Plug-Flow detention time= 940.6 min calculated for 0.003 af (7% of inflow) Center-of-Mass det. time= 507.6 min (1,246.6 - 739.0)

<u>Volume</u>	Inv	ert Ava	il.Storage	Storage Descrip	otion	
#1	85.	99'	1,823 cf	Custom Stage	Data (Prismatic)	Listed below (Recalc)
Elevation		Cumf Area	\/aida	In a Ohana	0	
		Surf.Area	Voids	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1,391	
90.50		864	100.0	432	1,823	
Device	Routing	ln	vert Out	et Devices		
#1	Primary	90	.00' 230.	.0' long x 1.0' bro	eadth Broad-Cres	sted Rectangular Weir
			Hea	d (feet) 0.20 0.4	0 0.60 0.80 1.00	0 1.20 1.40 1.60 1.80 2.00
				3.00		1100 2100
			Coe	f. (English) 2.69	2.72 2.75 2.85	2.98 3.08 3.20 3.28 3.31

Primary OutFlow Max=0.01 cfs @ 18.21 hrs HW=90.00' TW=85.30' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.06 fps)

3.30 3.31 3.32

Type III 24-hr 50-YR STORM Rainfall=7.48"

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Outflow=0.04 cfs 0.010 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

reachioung	by byn-otor-n	id method - Fond	routing by D	y11-3101-11	ia methoa	
Subcatchment 10S: Subcat		Runoff Area=531, w Length=1,150' To				
Subcatchment 11S: Subcat	chment 11S	Runoff Area=60,4 Flow Length=611'				
Subcatchment 12S: Subcat	chment 11S	Runoff Area=127,9 Flow Length=736' 7				
Subcatchment 13S: Subcat	chment 13S	Runoff Area=14,3			ous Runoff I Runoff=1.92	
Subcatchment 20S: Subcat		Runoff Area=240, Flow Length=627' T	429 sf 5.06° c=9.5 min (% Impervio	ous Runoff I unoff=20.84	Depth>3.69" cfs 1.696 af
Subcatchment 112S: PR HC	OUSE	Runoff Area=3,00			ous Runoff [Runoff=0.58 c	
Subcatchment 113S: PR HC	OUSE	Runoff Area=3,00			ous Runoff L Runoff=0.58 d	
Subcatchment 115S: PR HC	OUSE	Runoff Area=3,00			ous Runoff [Runoff=0.58 c	
Subcatchment 117S: PR HC	USE	Runoff Area=3,000			ous Runoff [Runoff=0.58 c	
Subcatchment 119S: PR HO	USE	Runoff Area=3,000			ous Runoff D Runoff=0.58 c	
Reach 1R: Analysis Point #1	I				nflow=47.18 c tflow=47.18 c	
Reach 2R: Analysis Point #2	2				nflow=25.88 c tflow=25.88 c	
Pond 1P: Pond 1P	12.0" Round	Peak Elev=83.30' Culvert n=0.013 L=				
Pond 2P: CB 1	15.0" Round	d Culvert n=0.013 L			Inflow=1.92 c utflow=1.92 c	
Pond 3P: CB 2	24.0" Round	Culvert n=0.013 L=			nflow=14.35 c tflow=14.35 c	
Pond 12P: DRIP EDGE		Peak Elev=90.0	00' Storage=	1,392 cf	Inflow=0.58 c	fs 0.042 af

Type III 24-hr 50-YR STORM Rainfall=7.48"

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Pond 14P: DRIP EDGE Peak Elev=90.00' Storage=1,392 cf Inflow=0.58 cfs 0.042 af

Outflow=0.04 cfs 0.010 af

Pond 16P: DRIP EDGE Peak Elev=90.00' Storage=1,392 cf Inflow=0.58 cfs 0.042 af

Outflow=0.04 cfs 0.010 af

Pond 18P: DRIP EDGE Peak Elev=90.00' Storage=1,392 cf Inflow=0.58 cfs 0.042 af

Outflow=0.04 cfs 0.010 af

Pond 20P: DRIP EDGE Peak Elev=90.00' Storage=1,392 cf Inflow=0.58 cfs 0.042 af

Outflow=0.04 cfs 0.010 af

Total Runoff Area = 22.731 ac Runoff Volume = 7.776 af Average Runoff Depth = 4.11" 91.49% Pervious = 20.797 ac 8.51% Impervious = 1.935 ac

Pond 12P: DRIP EDGE

Peak Elev=90.01' Storage=1,396 cf Inflow=0.69 cfs 0.050 af

Outflow=0.28 cfs 0.018 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

reach routing i	by Dyll-Otol-i	ind method - 1 ond routing by byn-otor-ind method
Subcatchment 10S: Subcate		Runoff Area=531,948 sf 4.81% Impervious Runoff Depth>5.42" low Length=1,150' Tc=12.6 min CN=71 Runoff=62.35 cfs 5.516 af
Subcatchment 11S: Subcate	chment 11S	Runoff Area=60,477 sf 15.00% Impervious Runoff Depth>6.16" Flow Length=611' Tc=11.2 min CN=77 Runoff=8.30 cfs 0.713 af
Subcatchment 12S: Subcato	chment 11S	Runoff Area=127,930 sf 12.65% Impervious Runoff Depth>5.30" Flow Length=736' Tc=8.5 min CN=70 Runoff=16.53 cfs 1.297 af
Subcatchment 13S: Subcatch	chment 13S	Runoff Area=14,396 sf 43.66% Impervious Runoff Depth>6.53" Tc=6.0 min CN=80 Runoff=2.42 cfs 0.180 af
Subcatchment 20S: Subcatc	chment 20S	Runoff Area=240,429 sf 5.06% Impervious Runoff Depth>4.93" Flow Length=627' Tc=9.5 min CN=67 Runoff=27.95 cfs 2.268 af
Subcatchment 112S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>8.73" Tc=0.0 min CN=98 Runoff=0.69 cfs 0.050 af
Subcatchment 113S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>8.73" Tc=0.0 min CN=98 Runoff=0.69 cfs 0.050 af
Subcatchment 115S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>8.73" Tc=0.0 min CN=98 Runoff=0.69 cfs 0.050 af
Subcatchment 117S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>8.73" Tc=0.0 min CN=98 Runoff=0.69 cfs 0.050 af
Subcatchment 119S: PR HO	USE	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>8.73" Tc=0.0 min CN=98 Runoff=0.69 cfs 0.050 af
Reach 1R: Analysis Point #1		Inflow=62.35 cfs 5.552 af Outflow=62.35 cfs 5.552 af
Reach 2R: Analysis Point #2		Inflow=33.80 cfs 4.476 af Outflow=33.80 cfs 4.476 af
Pond 1P: Pond 1P	12.0" Round	Peak Elev=84.24' Storage=30,592 cf Inflow=26.56 cfs 2.208 afd Culvert n=0.013 L=110.0' S=0.0655 '/' Outflow=7.32 cfs 2.172 af
Pond 2P: CB 1	15.0" Rour	Peak Elev=88.67' Inflow=2.42 cfs 0.180 af nd Culvert n=0.013 L=50.0' S=0.0050 '/' Outflow=2.42 cfs 0.180 af
Pond 3P: CB 2	24.0" Round	Peak Elev=88.53' Inflow=18.84 cfs 1.496 af d Culvert n=0.013 L=52.0' S=0.0048 '/' Outflow=18.84 cfs 1.496 af

Type III 24-hr 100-YR STORM Rainfall=8.97"

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Pond 14P: DRIP EDGE Peak Elev=90.01' Storage=1,396 cf Inflow=0.69 cfs 0.050 af

Outflow=0.28 cfs 0.018 af

Pond 16P: DRIP EDGE Peak Elev=90.01' Storage=1,396 cf Inflow=0.69 cfs 0.050 af

Outflow=0.28 cfs 0.018 af

Pond 18P: DRIP EDGE Peak Elev=90.01' Storage=1,396 cf Inflow=0.69 cfs 0.050 af

Outflow=0.28 cfs 0.018 af

Pond 20P: DRIP EDGE Peak Elev=90.01' Storage=1,396 cf Inflow=0.69 cfs 0.050 af

Outflow=0.28 cfs 0.018 af

Total Runoff Area = 22.731 ac Runoff Volume = 10.224 af Average Runoff Depth = 5.40" 91.49% Pervious = 20.797 ac 8.51% Impervious = 1.935 ac HydroCAD® 10.00-20 s/n 03433 © 2017 HydroCAD Software Solutions LLC

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Summary for Subcatchment 10S: Subcatchment 10S

Runoff

62.35 cfs @ 12.17 hrs, Volume=

5.516 af, Depth> 5.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

A	rea (sf)	CN E	Description						
	3,413	98 F	98 Roofs, HSG B						
	14,383	98 F	98 Roofs, HSG C						
	7,767	98 F	Paved road	s w/curbs &	& sewers, HSG C				
	98,769	61 >	75% Gras	s cover, Go	ood, HSG B				
2	260,481				ood, HSG C				
	30,102			od, HSG B					
1	17,033	70 V	<u>Voods, Go</u>	<u>od, HSG C</u>					
	531,948		Veighted A	-					
	06,385	_		vious Area					
	25,563	4	.81% Impe	ervious Area	a				
_		01			B				
	Length	Slope	Velocity		Description				
(min)	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)					
0.2	10	0.0200	0.87		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.23"				
2.7	40	0.0800	0.25		Sheet Flow,				
0.0	455	0.0050	4.44		Grass: Short n= 0.150 P2= 3.23"				
2.3	155	0.0250	1.11		Shallow Concentrated Flow,				
5.1	550	0.0650	1.78		Short Grass Pasture Kv= 7.0 fps				
J. I	550	0.0000	1.70		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				
2.3	395	0.0350	2.81		Shallow Concentrated Flow,				
2.0	333	0.0550	2.01		Grassed Waterway Kv= 15.0 fps				
12.6	1,150	Total			Oldosod Waterway IN- 10.0 Ips				
12.0	1,150	Total							

Summary for Subcatchment 11S: Subcatchment 11S

Runoff

8.30 cfs @ 12.16 hrs, Volume=

0.713 af, Depth> 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

Area (sf)	CN	Description
3,900	98	Paved roads w/curbs & sewers, HSG B
5,174	98	Paved roads w/curbs & sewers, HSG C
1,866	61	>75% Grass cover, Good, HSG B
42,233	74	>75% Grass cover, Good, HSG C
7,304	70	Woods, Good, HSG C
60,477	77	Weighted Average
51,403		85.00% Pervious Area
9,074		15.00% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	5.6	50	0.0200	0.15	,	Sheet Flow,
						Grass: Short n= 0.150 P2= 3.23"
	5.3	495	0.0500	1.57		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.2	36	0.0200	2.87		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	0.1	30	0.3300	4.02		Shallow Concentrated Flow,
_						Short Grass Pasture Kv= 7.0 fps
	11.2	611	Total			

Summary for Subcatchment 12S: Subcatchment 11S

Runoff = 16.53 cfs @ 12.12 hrs, Volume=

1.297 af, Depth> 5.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

_	A	rea (sf)	CN I	Description							
		5,122	98 I	98 Roofs, HSG B							
		6,235	98 I	98 Paved roads w/curbs & sewers, HSG B							
		4,824	98	Paved road	s w/curbs &	& sewers, HSG C					
		63,142		>75% Grass cover, Good, HSG B							
		41,943				ood, HSG C					
_		6,664	70 \	<u> Voods, Go</u>	od, HSG C						
		27,930		Neighted A							
	1	11,749			vious Area						
		16,181	1	12.65% lmp	pervious Ar	ea					
	_		-								
	Tc	_	Slope		Capacity	Description					
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	0.2	13	0.0200	0.92		Sheet Flow,					
						Smooth surfaces n= 0.011 P2= 3.23"					
	3.3	37	0.0400	0.18		Sheet Flow,					
	0.0	400	0.0400	4.00		Grass: Short n= 0.150 P2= 3.23"					
	2.0	120	0.0400	1.00		Shallow Concentrated Flow,					
	2.5	244	0.0400	4.40		Woodland Kv= 5.0 fps					
	2.5	211	0.0400	1.40		Shallow Concentrated Flow,					
	0.5	355	0.0325	12.38	173.39	Short Grass Pasture Kv= 7.0 fps					
	0.5	300	0.0323	12.30	173.39	Trap/Vee/Rect Channel Flow, Bot.W=1.00' D=2.00' Z= 3.0 '/' Top.W=13.00'					
						n= 0.022 Earth, clean & straight					
-	8.5	736	Total			11- 0.022 Lartii, Cleari & Straight					
	0.0	130	Total								

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Summary for Subcatchment 13S: Subcatchment 13S

Runoff

2.42 cfs @ 12.09 hrs, Volume=

0.180 af, Depth> 6.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

A	rea (sf)	CN I	N Description							
	3,684	98	Paved road	s w/curbs &	& sewers, HSG B					
	2,602	98	Paved road	s w/curbs &	& sewers, HSG C					
	4,639	61 :	>75% Gras	s cover, Go	Good, HSG B					
	3,471	74 :	>75% Gras	s cover, Go	lood, HSG C					
	14,396	80 \	80 Weighted Average							
	8,110		56.34% Pervious Area							
	6,286	43.66% Impervious Area								
Тс	Length	Slope	Velocity	Capacity	Description					
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)						
6.0					Direct Entry,					

Summary for Subcatchment 20S: Subcatchment 20S

Runoff

27.95 cfs @ 12.14 hrs, Volume=

2.268 af, Depth> 4.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

Area (s	f) CN	Description
3,68	5 98	Roofs, HSG B
3,57	1 98	Roofs, HSG C
2,70	3 98	Paved roads w/curbs & sewers, HSG B
2,21	8 98	Paved roads w/curbs & sewers, HSG C
75,01	6 61	>75% Grass cover, Good, HSG B
50,50	0 74	>75% Grass cover, Good, HSG C
37,55	0 55	Woods, Good, HSG B
65,18	6 70	Woods, Good, HSG C
240,42	9 67	Weighted Average
228,25	2	94.94% Pervious Area
12,17	7	5.06% Impervious Area

Type III 24-hr 100-YR STORM Rainfall=8.97"

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_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.3	17	0.0200	0.97		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.23"
	2.1	33	0.1000	0.26		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.23"
	2.5	165	0.0500	1.12		Shallow Concentrated Flow,
	4.5					Woodland Kv= 5.0 fps
	4.6	412	0.0900	1.50		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	9.5	627	Total			

Summary for Subcatchment 112S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 0.69 cfs @ 12.00 hrs, Volume=

0.050 af, Depth> 8.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

Area (sf)	CN	Description	
2,500	98	Roofs, HSG C	
500	98	Paved parking, HSG C	
3,000 3,000	98	Weighted Average 100.00% Impervious Area	

Summary for Subcatchment 113S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 0.69 cfs @ 12.00 hrs, Volume=

0.050 af, Depth> 8.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

 Area (sf)	CN	Description
2,500	98	Roofs, HSG C
500	98	Paved parking, HSG C
3,000 3,000	98	Weighted Average 100.00% Impervious Area

Summary for Subcatchment 115S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 0.69 cfs @ 12.00 hrs, Volume=

0.050 af, Depth> 8.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

Type III 24-hr 100-YR STORM Rainfall=8.97"

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Area (sf)	CN	Description		
2,500	98	Roofs, HSG C		
500	98	Paved parking, HSG C		
3,000 3,000	98	Weighted Average 100.00% Impervious Area		

Summary for Subcatchment 117S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.69 cfs @ 12.00 hrs, Volume=

0.050 af, Depth> 8.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

Area (sf)	CN	Description
2,500	98	Roofs, HSG C
500	98	Paved parking, HSG C
3,000 3,000	98	Weighted Average 100.00% Impervious Area

Summary for Subcatchment 119S: PR HOUSE

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff

0.69 cfs @ 12.00 hrs, Volume=

0.050 af, Depth> 8.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR STORM Rainfall=8.97"

Area (sf)	CN	Description	
2,500	98	Roofs, HSG C	
500	98	Paved parking, HSG C	
3,000	98	Weighted Average	
3,000		100.00% Impervious Area	

Summary for Reach 1R: Analysis Point #1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

12.350 ac, 5.87% Impervious, Inflow Depth > 5.40" for 100-YR STORM event

Inflow Outflow

62.35 cfs @ 12.17 hrs, Volume= 5.552 af

62.35 cfs @ 12.17 hrs, Volume= 5.552 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs. dt= 0.05 hrs.

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Summary for Reach 2R: Analysis Point #2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.382 ac, 11.66% Impervious, Inflow Depth > 5.17" for 100-YR STORM event

Inflow = 33.80 cfs @ 12.14 hrs, Volume= 4.476 af

Outflow = 33.80 cfs @ 12.14 hrs, Volume= 4.476 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1P: Pond 1P

Inflow Area = 4.725 ac, 16.78% Impervious, Inflow Depth > 5.61" for 100-YR STORM event

Inflow = 26.56 cfs @ 12.13 hrs, Volume= 2.208 af

Outflow = 7.32 cfs @ 12.54 hrs, Volume= 2.172 af, Atten= 72%, Lag= 25.1 min

Primary = 7.32 cfs @ 12.54 hrs, Volume= 2.172 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 84.24' @ 12.54 hrs Surf.Area= 9,362 sf Storage= 30,592 cf

Plug-Flow detention time= 53.1 min calculated for 2.167 af (98% of inflow)

Avoil Storage Storage Description

Center-of-Mass det. time= 43.3 min (859.6 - 816.3)

volume	invert Av	all.Storage	Storage Descripti	on	
#1	80.00'	37,994 cf	Custom Stage D	ata (Irregular) Lis	ted below (Recald
Elevation (feet)	Surf.Area (sq-ft		Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
80.00 82.00	5,262 7,037		0 12,256	0	5,262
84.00	9,096		16,089	12,256 28,345	7,133 9,492
85.00	10,213	377.4	9,649	37,994	10,739
Device Rou	tina	nvert Outl	et Devices		

#1 Primary 80.00' 12.0" Round Culvert

L= 110.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 80.00' / 72.80' S= 0.0655 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=7.32 cfs @ 12.54 hrs HW=84.24' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 7.32 cfs @ 9.31 fps)

Summary for Pond 2P: CB 1

Inflow Area = 0.330 ac, 43.66% Impervious, Inflow Depth > 6.53" for 100-YR STORM event

Inflow = 2.42 cfs @ 12.09 hrs, Volume= 0.180 af

Outflow = 2.42 cfs @ 12.09 hrs, Volume= 0.180 af, Atten= 0%, Lag= 0.0 min

Primary = 2.42 cfs @ 12.09 hrs. Volume= 0.180 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 100-YR STORM Rainfall=8.97"

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Peak Elev= 88.67' @ 12.16 hrs

Flood Elev= 89.80'

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=87.70' TW=88.28' (Dynamic Tailwater)
1=Culvert (Controls 0.00 cfs)

Summary for Pond 3P: CB 2

[80] Warning: Exceeded Pond 2P by 0.62' @ 12.10 hrs (3.67 cfs 0.044 af)

Inflow Area = 3.336 ac, 17.52% Impervious, Inflow Depth > 5.38" for 100-YR STORM event

Inflow = 18.84 cfs @ 12.12 hrs, Volume= 1.496 af

Outflow = 18.84 cfs @ 12.12 hrs, Volume= 1.496 af, Atten= 0%, Lag= 0.0 min

Primary = 18.84 cfs @ 12.12 hrs, Volume= 1.496 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 88.53' @ 12.12 hrs

Flood Elev= 89.80'

Device Routing Invert Outlet Devices

#1 Primary

85.05'

24.0" Round Culvert

L= 52.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 85.05' / 84.80' S= 0.0048 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=18.34 cfs @ 12.12 hrs HW=88.41' TW=82.66' (Dynamic Tailwater) 1=Culvert (Inlet Controls 18.34 cfs @ 5.84 fps)

Summary for Pond 12P: DRIP EDGE

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=3)

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 8.73" for 100-YR STORM event

Inflow = 0.69 cfs @ 12.00 hrs, Volume= 0.050 af

Outflow = 0.28 cfs @ 12.30 hrs, Volume= 0.018 af, Atten= 59%, Lag= 18.3 min

Primary = 0.28 cfs @ 12.30 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.01' @ 12.30 hrs Surf.Area= 864 sf Storage= 1,396 cf

Plug-Flow detention time= 367.4 min calculated for 0.018 af (36% of inflow)

Center-of-Mass det. time= 189.2 min (923.5 - 734.3)

Type III 24-hr 100-YR STORM Rainfall=8.97"

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Volume	Inv	vert Ava	il.Storage	Storage Descri	iption	
#1	85.	99'	1,823 cf	Custom Stage	Data (Prismatic	Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1,391	
90.5	50	864	100.0	432	1,823	
Device #1	Routing Primary	90.00' 2 H		ad (feet) 0.20 0.4 0 3.00	40 0.60 0.80 1.0	ested Rectangular Weir 00 1.20 1.40 1.60 1.80 2.00 2.98 3.08 3.20 3.28 3.31
				3.31 3.32		

Primary OutFlow Max=0.26 cfs @ 12.30 hrs HW=90.01' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.20 fps)

Summary for Pond 14P: DRIP EDGE

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=3)

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 8.73" for 100-YR STORM event 0.69 cfs @ 12.00 hrs, Volume= 0.050 af 0.28 cfs @ 12.30 hrs, Volume= 0.018 af, Atten= 59%, Lag= 18.3 min 0.28 cfs @ 12.30 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.01' @ 12.30 hrs Surf.Area= 864 sf Storage= 1,396 cf

Plug-Flow detention time= 367.4 min calculated for 0.018 af (36% of inflow) Center-of-Mass det. time= 189.2 min (923.5 - 734.3)

Volume	Inv	ert Ava	il.Storage	Storage Descrip	otion	
#1	85.	99'	1,823 cf	Custom Stage	Data (Prismatic) Listed b	elow (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1 ,391	
90.5	50	864	100.0	432	1,823	
Device	Routing	In		et Devices		
#1	Primary	90).00' 230 .	0' long x 1.0' br	eadth Broad-Crested Re	ctangular Weir

230.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00

Type III 24-hr 100-YR STORM Rainfall=8.97"

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Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Primary OutFlow Max=0.26 cfs @ 12.30 hrs HW=90.01' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.20 fps)

Summary for Pond 16P: DRIP EDGE

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=3)

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 8.73" for 100-YR STORM event

Inflow = 0.69 cfs @ 12.00 hrs, Volume= 0.050 af

Outflow = Primary = 0.28 cfs @ 12.30 hrs, Volume= 0.018 af, Atten= 59%, Lag= 18.3 min 0.28 cfs @ 12.30 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.01' @ 12.30 hrs Surf.Area= 864 sf Storage= 1,396 cf

Plug-Flow detention time= 367.4 min calculated for 0.018 af (36% of inflow)

Center-of-Mass det. time= 189.2 min (923.5 - 734.3)

Volume	Inv	ert Ava	il.Storage	Storage Descrip	otion	
#1	85.	99'	1,823 cf	Custom Stage	Data (Prismatic)	Listed below (Recalc)
Elevation	an.	Surf.Area	Voids	Inc.Store	Cum Stone	
	-				Cum.Store	
(fee		(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1,391	
90.5	50	864	100.0	432	1,823	
Device	Routing	In	vert Out	let Devices		
#1	Primary	90	0.00' 230	.0' long x 1.0' br	eadth Broad-Cre	ested Rectangular Weir
	•					00 1.20 1.40 1.60 1.80 2.00
				3.00		
			Coe	ef. (English) 2.69	2.72 2.75 2.85	2.98 3.08 3.20 3.28 3.31

Primary OutFlow Max=0.26 cfs @ 12.30 hrs HW=90.01' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.20 fps)

3.30 3.31 3.32

Summary for Pond 18P: DRIP EDGE

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=3)

Inflow Area =	=	0.069 ac,100.00% Impervious, Inflow Depth > 8.73" for 100-YR STORM event
Inflow =		0.69 cfs @ 12.00 hrs, Volume= 0.050 af
Outflow =		0.28 cfs @ 12.30 hrs, Volume= 0.018 af, Atten= 59%, Lag= 18.3 min
Primary =		0.28 cfs @ 12.30 hrs. Volume= 0.018 af

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.01' @ 12.30 hrs Surf.Area= 864 sf Storage= 1,396 cf

Plug-Flow detention time= 367.4 min calculated for 0.018 af (36% of inflow)

Center-of-Mass det. time= 189.2 min (923.5 - 734.3)

Volume	Inv	<u>vert</u> Ava	il.Storag	e Storage Desci	ription	
#1	85.	99'	1,823	cf Custom Stage	e Data (Prismatic	Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.9	99	864	0.0	0	0	
86.0	00	864	40.0	3	3	
89.9	99	864	40.0	1,379	1,382	
90.0	00	864	100.0	9	1,391	
90.5	50	864	100.0	432	1,823	
Device #1	Routing			outlet Devices 30.0' long x 1.0' b	oreadth Broad-Cr	ested Rectangular Weir
					.40 0.60 0.80 1.0	00 1.20 1.40 1.60 1.80 2.00
				50 3.00		
				oef. (English) 2.69 30 3.31 3.32	9 2.72 2.75 2.85	5 2.98 3.08 3.20 3.28 3.31

Primary OutFlow Max=0.26 cfs @ 12.30 hrs HW=90.01' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.20 fps)

Summary for Pond 20P: DRIP EDGE

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=3)

Inflow Area = 0.069 ac,100.00% Impervious, Inflow Depth > 8.73" for 100-YR STORM event

Inflow = 0.69 cfs @ 12.00 hrs, Volume= 0.050 af

Outflow = 0.28 cfs @ 12.30 hrs, Volume= 0.018 af, Atten= 59%, Lag= 18.3 min

Primary = 0.28 cfs @ 12.30 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.01' @ 12.30 hrs Surf.Area= 864 sf Storage= 1,396 cf

Plug-Flow detention time= 367.4 min calculated for 0.018 af (36% of inflow)

Center-of-Mass det. time= 189.2 min (923.5 - 734.3)

Volume	Invert	Avail.Storage	Storage Description
#1	85.99'	1,823 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Type III 24-hr 100-YR STORM Rainfall=8.97"

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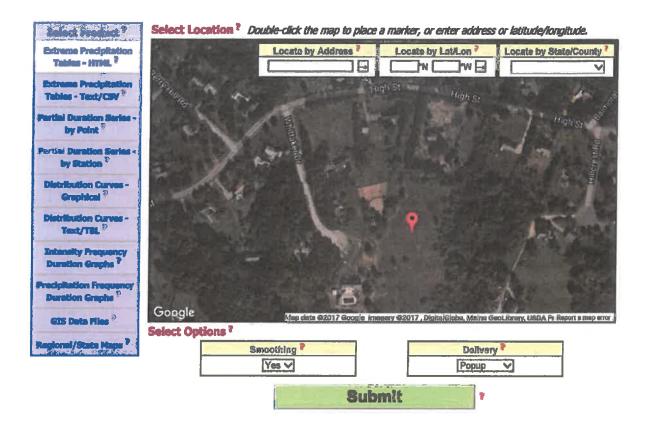
Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
85.99	864	0.0	0	0
86.00	864	40.0	3	3
89.99	864	40.0	1,379	1,382
90.00	864	100.0	9	1,391
90.50	864	100.0	432	1,823

Device	Routing	Invert	Outlet Devices
#1	Primary		230.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.26 cfs @ 12.30 hrs HW=90.01' TW=86.90' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.20 fps)

APPENDIX III

Charts, Graphs, and Calculations



Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing

State

New Hampshire

Location

Longitude 70.870 degrees West

Latitude

43.024 degrees North

Elevation

0 feet

Date/Time Tue, 27 Jun 2017 15:12:58 -0400

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1уг	0.26	0.40	0.50	0.66	0.82	1.04	1уг	0.71	0.99	1.22	1.57	2.04	2.68	2.93	1yr	2.38	2.82	3.23	3.95	4.57	1yr
2уг	0.32	0.50	0.62	0.81	1.02	1.30														5.35	
5yr	0.37	0.58	0.73	0.97	1.25	1.61														6.75	
10yr	0.41	0.65	0.82	1.11	1.45	1.89	10yr	1.25	1.72	2.23	2.90	3.77	4.91	5.57	10yr	4.35	5.36	6.12	7.17	8.05	10yr
25yr	0.48	0.76	0.97	1,33	1.77	2.34	25уг	1.53	2.14	2.78	3.65	4.77	6.24	7.16	25уг	5.52	6.89	7.85	9.13	10.17	25yr
50yr	0.54	0.86	1.10	1.54	2.07	2.76	50yr	1.79	2.52	3.29	4.34	5.71	7.48	8.67	50yr	6.62	8.33	9.49	10.96	12,14	50yr
100yr	0.59	0.96	1.24	1.77	2.42	3.26	100yr	2.08	2.97	3.91	5.19	6.83	8.97	10.49	100yr	7.94	10,09	11.46	13,16	14.50	100уг
200yr	0.67	1.10	1.42	2.04	2.82	3.84	200yr	2.44	3.51	4.63	6.17	8.16	10.77	12.70	200уг	9.53	12.21	13.85	15.82	17.33	200уг
500yr	0.80	1.31	1.71	2.48	3.47	4.77	500yr	3.00	4.38	5.78	7.76	10.33	13.70	16.35	500yr	12,12	15.72	17.81	20.18	21.94	500уг

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		Iday	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.73	0.89	1yr	0.63	0.87	0.92	1.30	1.62	2.22	2.62						3.92	
2yr	0.32	0.49	0.60	0.81	1.00	1.19								3.50			_			5.10	
5уг	0.35	0.54	0.68	0.93	1.18	1.41	5ут	1.02	1.38	1.62	2.13	2.74	3.85	4.29	5yr	3.41	4.13	4.77	5.64	6.36	5yr
10yr	0.39	0.60	0.74	1.04	1.34	1.61	10yr	1.16	1.58	1.82	2.40	3.08	4.45	5.01	10yr	3.94	4.82	5.59	6.57	7.36	10yr
25уг	0.45	0.68	0.85	1.21	1.59	1.92	25yr	1.37	1.88	2.11	2.78	3.57	4.76	6.14	25ут	4.21	5.90	6.90	8.06	8.94	25yr
50yr	0.49	0.75	0.94	1.35	1.81	2.20	50уг	1.56	2.15	2.36	3.11	3.99	5.38	7.15	50уг	4.76	6.87	8,10	9.41	10.35	50yr
100уг	0.55	0.84	1.05	1.52	2.08	2.52	100yr	1.80	2.46	2.64	3.46	4,44	6.05	8.32	100yr	5.35	8.00	9.53	10.99	11.97	100yr
200уг	0.62	0.93	1.18	1.71	2.38	2.88	200yr	2.05	2.81	2.95	3,84	4.92	6.78	9.69	200yr	6.00	9.32	11,22	12,84	13.88	200уг
500yr	0.72	1.08	1.39	2.01	2.87	3.46	500yr	2.47	3.38	3.44	4.40	5.67	7.88	11.86	500уг	6.98	11.40	13.94	15.80	16.82	500уг

Upper Confidence Limits

PP														_							
	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12br	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.44	0.54	0.72	0.89	1.08	1yr	0.77	1.06	1.26	1.74	2.20	3.02	3.11	1yr	2.67	2.99	3.62	4.37	5.09	1yr
2yr	0.33	0.51	0.63	0.86	1.06	1.26							3.45							5.68	
5yr	0.40	0.62	0.76	1.05	1.33	1.61	5yr	1.15	1.58	1.87	2.51	3.21	4.36	4.91	5yr	3.86	4.72	5.38	6.33	7.13	5yr
10yr	0.47	0.72	0.89	1.24	1.61	1.97	10yr	1.39	1.92	2.26	3.07	3.88	5.37	6.11	10yr	4.76	5.88	6.68	7.79	8.69	10yr
25yr	0.57	0.87	1.08	1.55	2.04	2.55	25yr	1.76	2.49	2.92	4.01	5.02	7.84	8.17	25yr	6.94	7.86	8.86	10.26	11.34	25уг
50уг	0.67	1.01	1.26	1.81	2.44	3.10	50уг	2.11	3.03	3.55	4.90	6.12	9.82	10.19	50yr	8.69	9.80	10.99	12.62	13.86	50yr
100yr				2.14		3.76	100yr	2.53	3.68	4.31	6.02	7.47	12.30	12.71	100yr	10.89	12.22	13.61	15.55	16.96	100уг
200yr	0.91	1.37	1.74	2.52	3.51	4.59	200yr	3.03	4.49	5.25	7.39	9.11	15.44	15.87	200yr	13.67	15.26	16.87	19.15	20.77	200ут
500yr	1.12	1.67	2.15	3.13	4.45																500yr



Michael Kerivan

From:

Jonathan Ring

Sent:

Monday, February 06, 2017 10:54 AM

To:

Katelyn Joyal

Cc:

Lynn Zebrowski; Paige Libbey; Patrick Bogle

Subject:

JBE 13070.1: Sullivan HISS, High Street, Stratham

Attachments:

Scanned image_copier@sbmweb.com_20170131_114946_0000f12e81b0.pdf

Kate - p/f/s/t. Jon

----Original Message----

From: Luke Hurley [mailto:lhurley@gesinc.biz] Sent: Tuesday, January 31, 2017 11:07 AM

To: Jonathan Ring

Subject: RE: Sullivan HISS

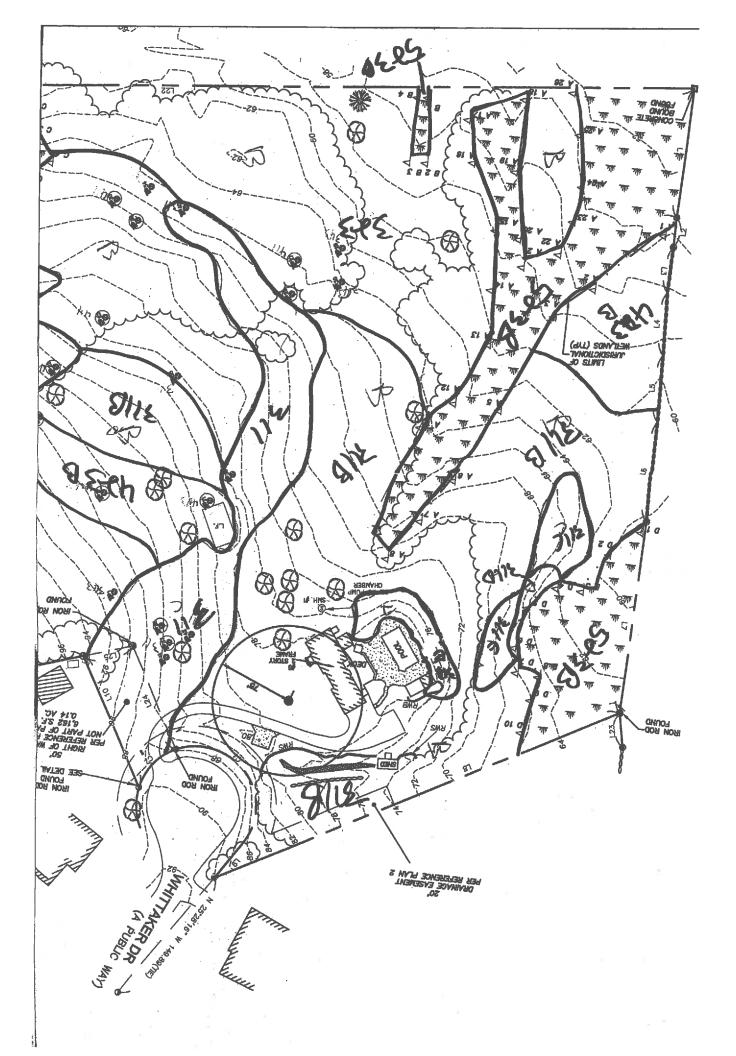
Here is the soil map. Please note when you mark it up to change the 323 to 343:

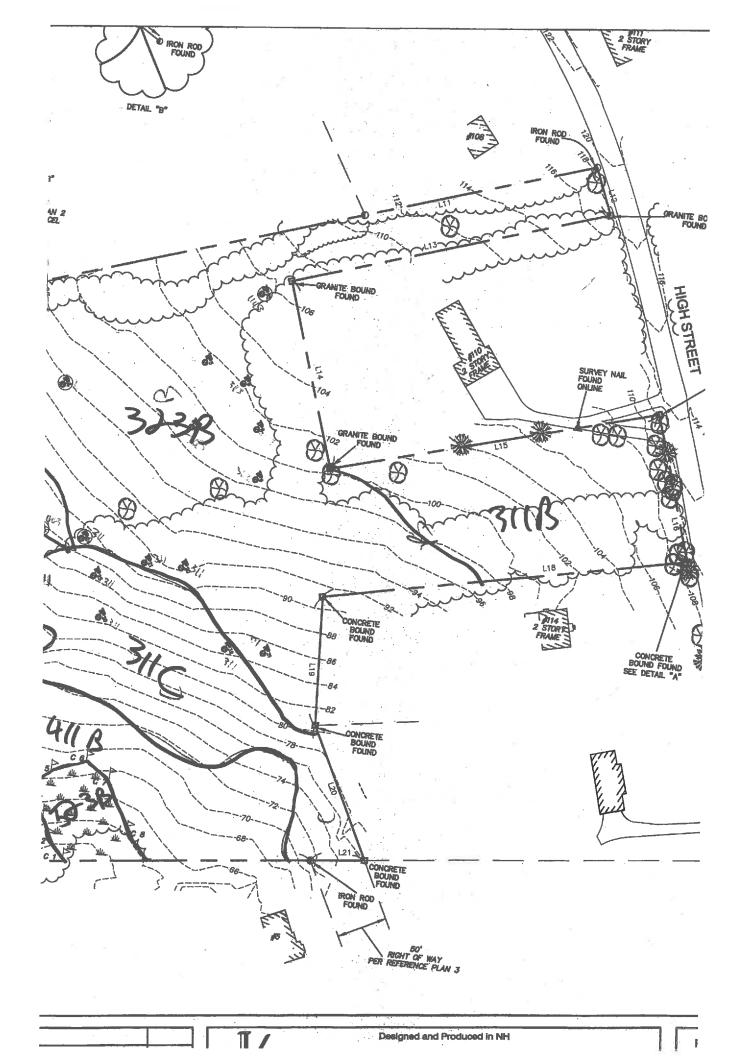
HISS SSSM

311 313 Deerfield HSG B 343 38 Eldridge HSG C

443 943 Eldridge Variant HSG C

523 656 Ridgebury HSG C







MAP LEGEND

Special Line Features Streams and Canals Very Stony Spot Stony Spot Spoil Area Wet Spot Other Water Features 8 Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Special Point Features Area of Interest (AOI) Blowout 3 Soils

Borrow Pit

Clay Spot

Rails Transportation #

Closed Depression

Interstate Highways Major Roads **US Routes**

Local Roads

Gravelly Spot

Gravel Pit

Aerial Photography

Marsh or swamp

Lava Flow

Landfill

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot Sandy Spot

Background

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of Warning: Soll Map may not be valid at this scale.

The soil surveys that comprise your AOI were mapped at

1:24,000.

MAP INFORMATION

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Coordinate System: Web Mercator (EPSG:3857) Web Soil Survey URL:

Maps from the Web Soil Survey are based on the Web Mercator distance and area. A projection that preserves area, such as the projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Rockingham County, New Hampshire Survey Area Data: Version 18, Sep 15, 2016

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jun 20, 2010-Jul The orthophoto or other base map on which the soil lines were 18, 2010

compiled and digitized probably differs from the background Imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Severely Eroded Spot

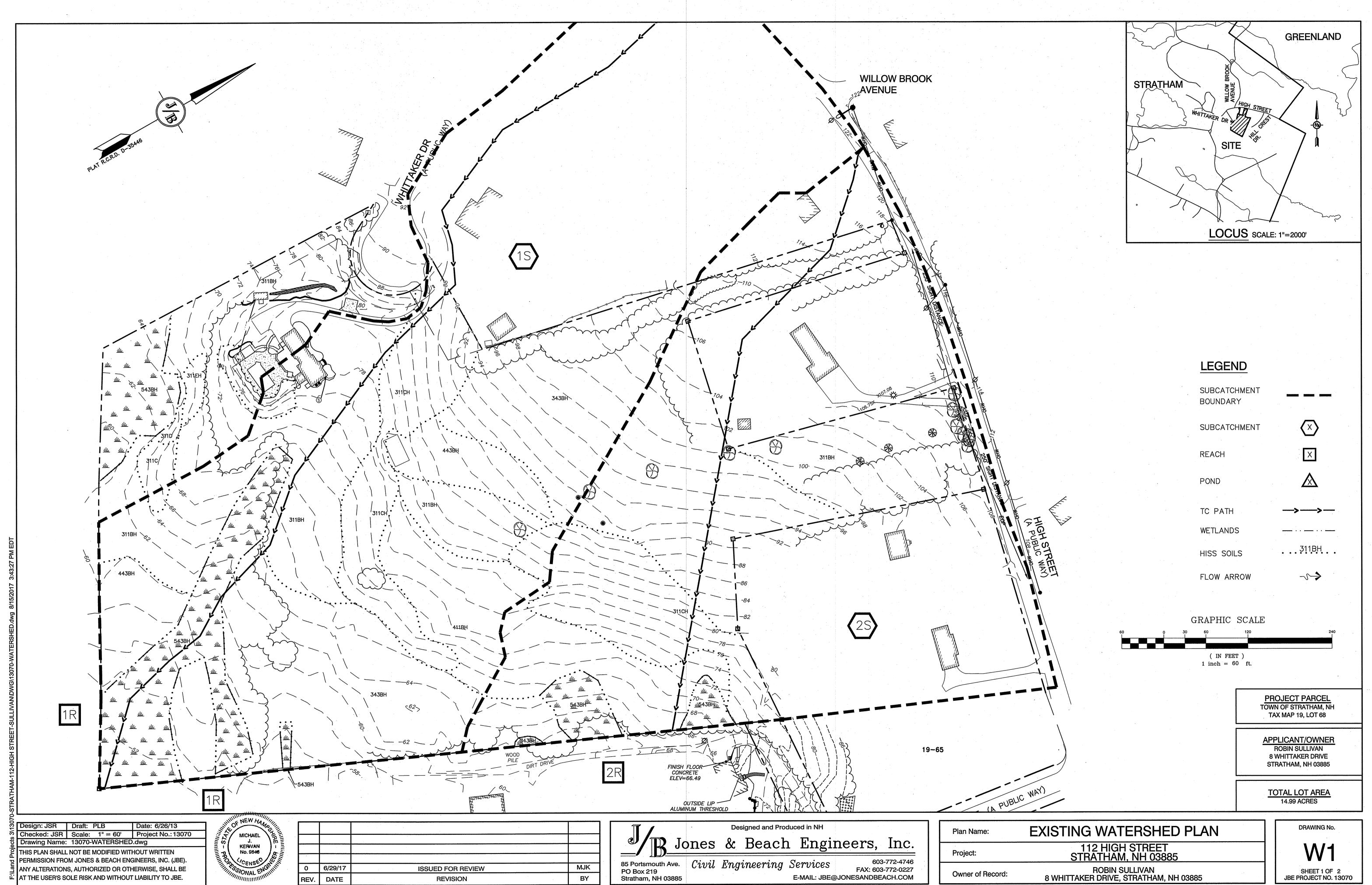
Slide or Slip

Sinkhole

Sodic Spot

Map Unit Legend

Rockingham County, New Hampshire (NH015)										
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI							
26B	Windsor loamy sand, 3 to 8 percent slopes	5.4	18.3%							
29B	Woodbridge fine sandy loarn, 3 to 8 percent slopes	10.8	36.4%							
32B	Boxford silt loam, 3 to 8 percent slopes	3.4	11.5%							
38A	Eldridge fine sandy loam, 0 to 3 percent slopes	4.2	14.0%							
510B	Hoosic gravelly fine sandy loam, 3 to 8 percent slopes	5.8	19.6%							
Totals for Area of Interest		29.6	100.0%							



AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

REV. DATE

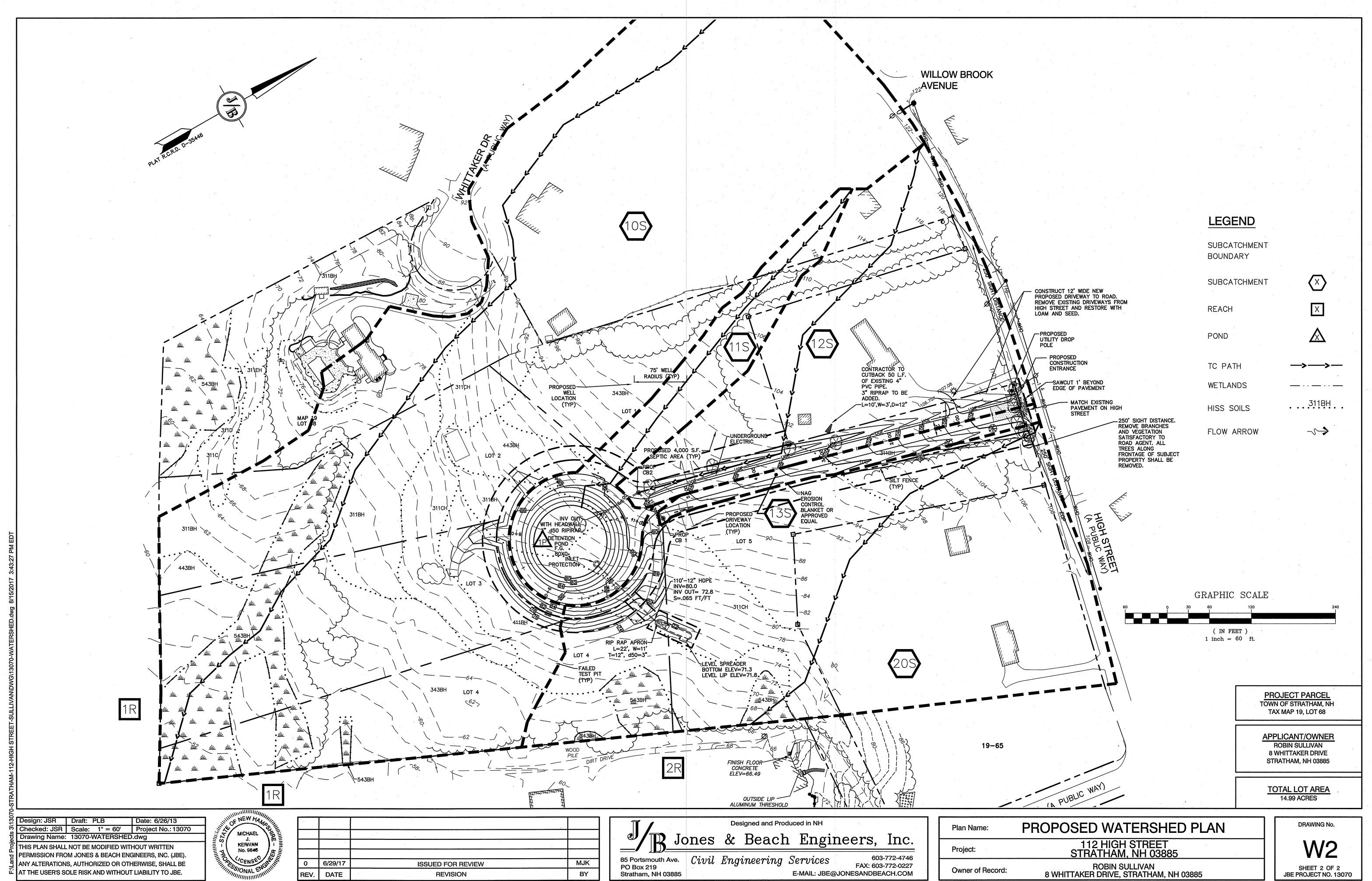
REVISION

BY

SHEET 1 OF 2 JBE PROJECT NO. 13070

Owner of Record:

E-MAIL: JBE@JONESANDBEACH.COM



THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

REV. DATE

REVISION

SHEET 2 OF 2 JBE PROJECT NO. 13070

Owner of Record:

CIVILWORKS NEW ENGLAND

181 WATSON ROAD P.O. BOX 1166 DOVER, NH 03821-1166

PHONE: (603) 750.4266 FAX: (603) 749.7348

September 14, 2017

Stratham Planning Board 10 Bunker Hill Avenue Stratham, NH 03885

Attn: Tavis Austin, Town Planner

(via email): TAustin@strathamNH.gov

Re: Subdivision Plan Review – Sullivan

Tax Map 19, Lot No. 68

112 High Street, Stratham, NH

Our Reference No. 1768

Dear Mr. Austin:

At your request, we have reviewed subdivision plans of the proposed Sullivan subdivision submitted by Jones & Beach Engineers, Inc. (JBE) in support of their application for Planning Board approval under subdivision review. The titles of the submitted plan sheets are listed below and are dated as noted:

PLAN NO.	TITLE	DATE	REV.
CS	Cover Sheet	8-16-17	2
A1	Subdivision Plan	8-16-17	2
C1	Existing Conditions Plan	8-16-17	2
C2	Grading and Drainage Plan	8-16-17	2
P1	Plan and Profile	8-16-17	2
D1	Detail Sheet	8-16-17	2
D2	Detail Sheet	8-16-17	2
E1	Erosion and Sediment Control Details	8-16-17	2

We are also in receipt of the above plan set noted as "Revision 1" and dated 7/5/17. Additionally, we have received plan sheets entitled "CONCEPTUAL SUBDIVISION PLAN" dated: 4/91/17 (Revision 1) and dated: 11/10/16 (Revision 0).

All plan sheets have been prepared by JBE. Also submitted were:

- 1. "DRAINAGE ANALYSIS SEDIMENT AND EROSION CONTROL PLAN", dated: June 29, 2017 and revised: August 16, 2017; as prepared by JBE.
- 2. Correspondence from JBE to the Stratham Planning Board dated: August 16, 2017.
- 3. "SITE PLAN REVIEW/SUBDIVISION WAIVER REQEUST FORM" requesting a 22' wide paved roadway width where 24' is required.
- 4. "LOT SIZE BY SOIL CLASSIFICATION" computations prepared by JBE and dated: August 16, 2017.
- 5. Logs of "TEST PITS FOR 8 WHITAKER DRIVE, STRATHAM, NEW HAMPSHIRE", APRIL 20, 2016; DECEMBER 14 & 27, 2016; as prepared by JBE.

The scope of our subdivision plan review includes:

- 1. Check for conformance with the Stratham Zoning Ordinance
- 2. Check for conformance with the Stratham Subdivision Regulations
- 3. Subdivision engineering and design review

As part of our review, we visited the subject site on August 22, 2017.

ZONING ORDINANCE CONFORMANCE REVIEW:

All appears to be in order. As such, we have no comments to share at this time.

SUBDIVISION REGULATIONS CONFORMANCE REVIEW:

- Section 3.3.2 states the scale of the "Subdivision Plan" should be no greater than 1"=50'.
 The submitted "subdivision plan" is at a scale of 1"=60' and as such, will require a WAIVER from the Regulations to be acceptable.
- 2. A plan and profile of existing conditions on High Street within 300' either side of the proposed roadway is required per Section 3.3.3(a.) of the Regulations.
- 3. Section 4.4.3 of the Regulations requires (in part) ".....the arrangement of streets in a subdivision shall provide for the continuation of the principal street existing in the adjoining subdivisions.....". The submitted CONCEPTUAL SUBDIVISION PLAN dated 4/19/17 provides for said continuation. The more recently submitted subdivision pan

- revisions do not provide for any continuation and instead, sets forth another dead end, cul-de-sac street proposal.
- 4. Section 4.5.3 addresses the (possible) need for a fire cistern at this proposed subdivision. The Planning Board should address this matter with the applicant.
- 5. TABLE 1 (p. 66) of the Regulations allows for a maximum centerline road grade of 2% in a cul-de-sac turnaround. The proposed roadway sets forth a centerline roadway grade of 3%. For this to be approvable by the Planning Board, a WAIVER from the Regulations will be required.

SUBDIVISION ENGINEERING AND DESIGN REVIEW:

- 1. A NHDOT specification should be shown and included for the "suitable clean fill" called for in the "TYPICAL ROADWAY SECTION" shown on plan sheet D1.
- 2. NHDES Subdivision Approval will be required for this subdivision proposal.
- 3. A "HISS" mapping legend should be provided on plan sheet C1 and C2 for proper interpretation of the "HISS" mapping data shown.
- 4. The available safe sight distances should be identified and shown for the proposed roadway's intersection with High Street.
- 5. We have no submitted data or logs for Soil Test Pits identified as #1 through #20 shown on plan sheets C1 and C2.
- 6. The stormwater drainage design appears to be satisfactory.
- 7. In general, we have no objections to the submitted WAIVER request. The Town Road Agent should be consulted for his input on the WAIVER request. Additionally, the Planning Board should give due consideration of the request as same relates to municipal policy and history relative to these matters.

RECOMMENDATIONS:

We have several reservations with regard to the Planning Board's consideration of approval for this subdivision. Our primary concerns are:

- 1. The proposal of a dead end cul-de-sac where alternatively, the continuation of existing streets; which will form a non-dead end "through street" and eliminate two (2) existing dead end cul-de-sacs would seem to be more logical, safer, and in closer alliance with the stated Subdivision Regulations of the Town.
- 2. Provision of a fire cistern for fire/life safety purposes.
- 3. The apparent limited safe sight distances at the proposed roadway's intersection with High Street.

The Board may wish to have the applicant address the comments contained herein prior to taking any action on the disposition of the plans.

Please feel free to contact me if there are any questions or comments regarding this subdivision review.

Very truly yours, CIVILWORKS, INC.

Paul J. Connolly, P.É., P.L.S.

PJC/lrd

cc: Jonathan Ring, P.E. (JBE), via email: jring@Jonesandbeach.com